

SUPERINTENDENCIA DE INDUSTRIA Y COMERCIO			
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DEP:	2020 DIRECCION DE NUEVAS CREACIONES	EVE:	379 FASE NACIONAL INCLUIDO CAPITULO II
TRA:	11 PCT-PATENTE DE INVENCION CAPITULOS I Y II	FOLIOS:	5
ACT:	519 PRESENTACION		

DIRECCIÓN DE NUEVAS CREACIONES

2020
Bogotá, D.C.,

Abogado(a)/Señor(a)
JUAN PABLO CADENA SARMIENTO

Asunto: Radicación: 11-168253- -4
 Trámite: 11
 Evento: 379
 Actuación: 519
 Oficio: 10260
 Folios: 5

Patente de Invención	X			Patente de Modelo de Utilidad	
Vía Nacional					
Vía PCT (Fase Nacional)	X	Capítulo I		Capítulo II	X
No. Solicitud Internacional	PCT/US2010/035560				
Fecha de Presentación Internacional	20/05/2010				

Como resultado del Examen de Fondo realizado, con fundamento en el Artículo 45 de la Decisión 486 de la Comisión de la Comunidad Andina, se comunica:

1. Documentos estudiados

Descripción:	Rad. Nº 11-168253-00000	06/Diciembre/2011
Reivindicaciones:	Rad. Nº 11-168253-00000	06/Diciembre/2011
Prioridades:	US 61/180,665	22/Mayo/2009

2. Análisis de la Prioridad

Se acepta la reivindicación de Prioridad porque esta solicitud fue presentada dentro del plazo establecido (Art. 9 D 486) y su contenido técnico corresponde con el de la prioridad reivindicada.

3. Objeto de la invención

De acuerdo con lo establecido en el numeral 1.2.2.2 del Capítulo Primero del Título X de la Circular Única para efectos del examen de patentabilidad, se tendrá en cuenta la tasa pagada por el solicitante al momento de comenzar el examen para las reivindicaciones adicionales; esto es que cuando la solicitud contenga más de diez (10)

reivindicaciones y no se haya pagado la tasa complementaria, sólo se estudiarán las cubiertas por la tasa pagada.

Se aceptan para estudio todas las 34 reivindicaciones presentadas (Fls. 58 a 64 del Rad. N° 11-168253-00000) porque las tasas pagadas cubren en su totalidad lo establecido en el numeral 1.2.2.2 del Capítulo Primero del Título X de la Circular Única.

Título de la solicitud: “composiciones cementicias de baja densidad” (Fl. 1).

El problema planteado en esta solicitud consiste en la necesidad de suministrar a formaciones subterráneas cemento que pueda formar paredes livianas.

Para resolver este problema técnico, la solicitud en estudio proporciona composiciones cementicias a base de polvo de horno cement klin dust CKD y micropartículas/microesferas.

El objeto de la presente Solicitud se relaciona con la Clasificación Internacional de Patentes (CIP) C04B 28/02.

4. De la Solicitud de Patente

Reivindicaciones (Art 30 D 486, Art 22 PCT)

Las reivindicaciones 1, 4, 5, 8, 10 a 13, 15, 16, 18, 19, 22, 25, 26, 32 y 34 no son claras porque las expresiones “*al menos*” y “*alrededor del*” son imprecisas, por lo cual no permiten distinguir la invención del estado de la técnica. Se sugiere sustituirlas por términos precisos o un rango concreto.

Las reivindicaciones 1 a 8, 13, 16 a 20, 22 a 27, 29 a 32 y 34 no son claras porque la expresiones “*resistencia compresiva*” y “*cuando se agrega con agua, en donde para una densidad*” y la densidad son resultados a alcanzar, lo que no está permitido, no define al producto y/o método porque la invención no queda definida por el resultado a alcanzar, puesto que la reivindicación incluiría no sólo la solución propuesta por el solicitante, sino todas las alternativas presentes o futuras que lleguen a ese resultado. Se sugiere remplazarla por las características esenciales estructurales que contribuyen a la obtención de ese efecto.

La reivindicaciones 1, 16, 22, 29 y 34 no son concisas porque las definiciones de aglutinante hidráulico, aditivo de peso ligero y polvo de horno para cemento, son géneros funcionales, se sugiere restringir la solicitud a una razonable generalización del tipo de compuestos que han sido sintetizados ó probados, es decir, que se encuentran debidamente sustentados.

La reivindicación 34 no es clara porque contiene el mismo objeto de la reivindicación 1, se sugiere eliminar dicha reivindicación.

5. Determinación del Estado de la Técnica

El estado de la técnica se determinó con base en la fecha de presentación de la solicitud de prioridad invocada, es decir, el 22 de mayo de 2009.

Consultadas las fuentes de información con que se cuenta, se encontraron los siguientes documentos que anticipan el objeto de esta solicitud.

Item	Documento	Título	Fecha de Publicación
D1	WO 2007/028952	“Settable compositions comprising cement kiln dust and additive(s) and method of using them”	15/Marzo/2007

D2	US 7335252	"Lightweight settable compositions comprising cement kiln dust"	26/Febrero/2008
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El documento D1¹ divulga composiciones cementables que contienen metacaolina y un método de uso de esa composición (Pág. 1, Párr. 1, Pág. 2, Párr. 7).

El documento D2² divulga composiciones cementables que contienen microesferas y un método de uso de esa composición (Col. 2, líneas 37 a 46).

6. Examen de Patentabilidad (Art 14 D486)

Novedad (Art 16 D486)

La reivindicación 16 consiste en *"Un aglutinante cementicio manufacturado que comprende: polvo de horno para cemento en una cantidad de..."* (Ver Fl. 60 del Rad. Nº 11-168253-00000).

Comparación de las características técnicas **esenciales**, con las del Estado de la Técnica:

Características esenciales	D1	D2
Aglutinante cementicio que comprende:	Composición cementicia que sella a base de polvo de horno CKD (Pág. 1, Párr. 1)	Composicion cementicia a a base de polvo de horno CKD y microesferas (Col. 2, líneas 37 a 46).
Polvo de horno para cemento en al menos 10% en peso y el polvo de horno para cemento incluye cloro mayor al 0.1% en peso del polvo de horno	Menos al 10 % en peso el polvo de horno, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso de KCl ³ (Pág. 24, Tabla 10).	La composición contiene entre un 5 y 50% de polvo de horno CKD (Col. 3, líneas 10 a 29).

De acuerdo con la tabla anterior, las características esenciales del método de la reivindicación 1 habían sido divulgadas previamente en los documentos D1 y D2, por lo tanto, la materia reivindicada no es nueva.

Las reivindicaciones dependientes 18 y 21 no mencionan alguna característica que haga nuevo el aglutinante cementicio de la reivindicación 16, por lo cual se considera que no son nuevas, ya que D2 divulga microesferas entre el 1 y el 30% en la composición, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso de KCl³ (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

Nivel inventivo (Art 18 D486)

La reivindicación 1 consiste en *"Un aglutinante cementicio manufacturado que comprende: un aglutinante hidráulico en una cantidad comprendida..."* (Ver Fl. 58 del Rad. Nº 11-168253-00000).

Comparación de las características técnicas **esenciales**, con las del Estado de la Técnica:

Características esenciales	D1	D2
Aglutinante cementicio que comprende:	Composición cementicia que sella a base de polvo de horno CKD (Pág. 1, Párr. 1)	Composicion cementicia a a base de polvo de horno CKD y microesferas (Col. 2, líneas 37 a 46).

¹[http://worldwide.espacenet.com/publicationDetails/biblio?](http://worldwide.espacenet.com/publicationDetails/biblio?DB=worldwide.espacenet.com&II=0&ND=3&adjacent=true&locale=en_EP&FT=D&date=20070315&CC=WO&NR=2007028952A1&KC=A1)

DB=worldwide.espacenet.com&II=0&ND=3&adjacent=true&locale=en_EP&FT=D&date=20070315&CC=WO&NR=2007028952A1&KC=A1

² <http://www.freepatentsonline.com/7335252.html>

³ Adaska WS and Taubert DH. Beneficial uses of cement kiln dust. Presented at 2008 IEEE/PCA 50th Cement Industry Technical Conf. Miami. Fl. May 19-22, 2008.

Aglutinante hidráulico entre alrededor del 40 y 75% en peso	El cemento hidráulico está entre el 20 y 95%, el cual puede ser cemento portland o cenizas volantes (Pág. 7, Párr. 24, Pág. 24, Tabla 10).	El cemento hidráulico se encuentra entre un 10 y 70% (Col. 4, líneas 26 a 44).
Metacaolina en al menos 3% en peso	La metacaolina está entre el 10 y el 50% (Pág. 8, Párr. 29).	No se menciona
Microsílica en hasta alrededor el 15% en peso	No se menciona	Contiene microesferas entre el 1 y el 30% y las microesferas pueden ser de ceniza volante, el cual es rico en silica (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).
Polvo de horno para cemento en al menos 10% en peso, y el polvo de horno para cemento incluye cloro mayor al 0.1% en peso del polvo de horno	Menos al 10 % en peso el polvo de horno, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso KCl ³ (Pág. 24, Tabla 10).	La composición contiene entre un 5 y 50% de polvo de horno CKD (Col. 3, líneas 10 a 29).

Los documentos D1 y D2 se consideran el estado de la técnica más cercano a la invención definida en la reivindicación 1, porque divulgan composiciones cementicias que contienen polvo de horno Cement Klin Dust CKD.

La diferencia entre la invención, definida en la reivindicación 1 y el aglutinante cementicio del documento D1 consiste en que D1 no menciona la microsílica.

La diferencia entre la invención, definida en la reivindicación 1 y el aglutinante cementicio del documento D2 consiste en que en D2 no se menciona la metacaolina.

El efecto que logra el incluir la microsílica es que permite crear una composición aglutinante de baja densidad lo que favorece la formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente.

Por lo tanto, el problema técnico objetivo que pretende resolver esta invención se puede formular así “¿cómo modificar la composición aglutinante de D1 para que se obtengan composiciones de baja densidad que permitan formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente?”.

Sin embargo, microesferas como lo son la microsilica, ya están divulgadas en el documento D2 que se refiere a composiciones aglutinantes cementicias a base de polvo de horno cement klin dust CKD (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

En consecuencia, una persona normalmente versada en la materia incluiría las microsílicas de D2 en la composición de la anterioridad D1, esperando con certeza lograr el producto, como la de la reivindicación 1 de la solicitud, lo cual es considerado obvio y, por lo tanto, sin altura inventiva.

Puesto que las reivindicaciones dependientes 4, 8 a 15 y 34 no mencionan características adicionales que hagan inventiva la solicitud, se considera que tales reivindicaciones tampoco tienen nivel inventivo, ya que D2 divulga la presencia de microesferas entre el 1 y el 30%, en donde las cenizas volantes que contienen la microsílica puede contener o no cal, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso de KCl³ (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

Conclusión:

Las reivindicaciones 1, 4, 8 a 15 y 34 cumplen el requisito de novedad (Art. 16), pero

no cumplen con el requisito de nivel inventivo (Art. 18).

La reivindicación 22 consiste en “Una composición cementicia fraguable que comprende: agua y un aglutinante cementicio que incluye:...” (Ver Fl. 61 del Rad. N° 11-168253-00000).

Comparación de las características técnicas **esenciales**, con las del Estado de la Técnica:

Características esenciales	D1	D2
Composición cementicia fraguable que comprende:	Composición cementicia que sella a base de polvo de horno CKD (Pág. 1, Párr. 1)	Composicion cementicia a a base de polvo de horno CKD y microesferas (Col. 2, líneas 37 a 46).
Agua y	Contiene agua (Pág. 1, Párr. 2)	Contiene agua (Col. 2, líneas 61 a 65).
Aglutinante cementicio que incluye:	Donde el sólido es el aglutinante (Pág. 1, Párr. 1)	Donde el sólido es el aglutinante (Col. 2, líneas 37 a 46).
Aglutinante hidráulico entre alrededor del 40 y 75% en peso	El cemento hidráulico está entre el 20 y 95%, el cual puede ser cemento portland o cenizas volantes (Pág. 7, Párr. 24, Pág. 24, Tabla 10).	El cemento hidráulico se encuentra entre un 10 y 70% (Col. 4, líneas 26 a 44).
Metacaolina en al menos 3% en peso	La metacaolina está entre el 10 y el 50% (Pág. 8, Párr. 29).	No se menciona
Microsílice en hasta alrededor el 15% en peso	No se menciona	Contiene microesferas entre el 1 y el 30% y las microesferas pueden ser de ceniza volante, el cual es rico en silica (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).
Polvo de horno para cemento en al menos 10% en peso y el polvo de horno para cemento incluye clora mayor al 0.1% en peso del polvo de horno	Menos al 10 % en peso el polvo de horno, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso KCl ³ (Pág. 24, Tabla 10).	La composición contiene entre un 5 y 50% de polvo de horno CKD (Col. 3, líneas 10 a 29).

Los documentos D1 y D2 se consideran el estado de la técnica más cercano a la invención definida en la reivindicación 22, porque divulgan composiciones cementicias que contienen polvo de horno Cement Klin Dust CKD.

La diferencia entre la invención, definida en la reivindicación 22 y la composición cementicia del documento D1 consiste en que D1 no menciona la microsílica.

La diferencia entre la invención, definida en la reivindicación 22 y la composición cementicia del documento D2 consiste en que en D2 no se menciona la metacaolina.

El efecto que logra el incluir la microsílica es que permite crear una composición aglutinante de baja densidad lo que favorece la formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente.

Por lo tanto, el problema técnico objetivo que pretende resolver esta invención se puede formular así “¿cómo modificar la composición aglutinante de D1 para que se obtengan composiciones de baja densidad que permitan formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente?”.

Sin embargo, microesferas como lo son la microsilica, ya están divulgadas en el

documento D2 que se refiere a composiciones aglutinantes cementicias a base de polvo de horno cement klin dust CKD (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

En consecuencia, una persona normalmente versada en la materia incluiría las microsílicas de D2 en la composición de la anterioridad D1, esperando con certeza lograr el producto, como la de la reivindicación 22 de la solicitud, lo cual es considerado obvio y, por lo tanto, sin altura inventiva.

Puesto que las reivindicaciones dependientes 25 y 28 no mencionan características adicionales que hagan inventiva la solicitud, se considera que tales reivindicaciones tampoco tienen nivel inventivo, ya que D2 divulga la presencia de microesferas entre el 1 y el 30%, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso de KCl³ (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

La reivindicación 29 consiste en “*Un método para cementación que comprende: proporcionar una composición cementicia fraguable que comprende: a) agua y b) un aglutinante cementicio que incluye:...*” (Ver Fl. 63 del Rad. N° 11-168253-00000).

Comparación de las características técnicas **esenciales**, con las del Estado de la Técnica:

Características esenciales	D1	D2
Método para cementación que comprende proporcionar:	Se proporciona a un pozo una composición cementable (Pág. 2, Párr. 7).	Se proporciona a una formación subterránea una composición cementable (Col. 2, líneas 37 a 46).
Una composición cementicia fraguable que comprende:	Composición cementicia que sella a base de polvo de horno CKD (Pág. 1, Párr. 1)	Composicion cementicia a a base de polvo de horno CKD y microesferas (Col. 2, líneas 37 a 46).
Agua y	Contiene agua (Pág. 1, Párr. 2)	Contiene agua (Col. 2, líneas 61 a 65).
Aglutinante cementicio que incluye:	Donde el sólido es el aglutinante (Pág. 1, Párr. 1)	Donde el sólido es el aglutinante (Col. 2, líneas 37 a 46).
Aglutinante hidráulico entre alrededor del 40 y 75% en peso	El cemento hidráulico está entre el 20 y 95%, el cual puede ser cemento portland o cenizas volantes (Pág. 7, Párr. 24, Pág. 24, Tabla 10).	El cemento hidráulico se encuentra entre un 10 y 70% (Col. 4, líneas 26 a 44).
Metacaolina en al menos 3% en peso	La metacaolina está entre el 10 y el 50% (Pág. 8, Párr. 29).	No se menciona
Microsílice en hasta alrededor el 15% en peso	No se menciona	Contiene microesferas entre el 1 y el 30% y las microesferas pueden ser de ceniza volante, el cual es rico en sílica (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).
Polvo de horno para cemento en al menos 10% en peso y el polvo de horno para cemento incluye cloro mayor al 0.1% en peso del polvo de horno	Menos al 10 % en peso el polvo de horno, siendo implícito para la persona versada en la materia que el CKD contiene en promedio 1.4% en peso KCl ³	La composición contiene entre un 5 y 50% de polvo de horno CKD (Col. 3, líneas 10 a 29).

	(Pág. 24, Tabla 10).	
E introducir la composición cementicia fraguable dentro de una formación subterránea	Se introduce la composición al pozo (Pág. 13, Párr. 44)	Se introduce la composición a la formación subterránea (Col. 7, líneas 53 a 65).

Los documentos D1 y D2 se consideran el estado de la técnica más cercano a la invención definida en la reivindicación 29, porque divulgan métodos de suministro de composiciones cementicias que contienen polvo de horno Cement Klin Dust CKD.

La diferencia entre la invención, definida en la reivindicación 29 y el método del documento D1 consiste en que D1 no menciona la microsíllica.

La diferencia entre la invención, definida en la reivindicación 29 y el método del documento D2 consiste en que en D2 no se menciona la metacaolina.

El efecto que logra el incluir la microsíllica es que permite crear una composición aglutinante de baja densidad lo que favorece la formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente.

Por lo tanto, el problema técnico objetivo que pretende resolver esta invención se puede formular así “¿cómo modificar el método de D1 para que se obtengan composiciones de baja densidad que permitan formación de paredes livianas en pozos de producción/perforación de hidrocarburos de forma más eficiente?”.

Sin embargo, microesferas como lo son la microsilica, ya están divulgadas en el documento D2 que se refiere a un método de suministro de composiciones aglutinantes cementicias a base de polvo de horno cement klin dust CKD (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9).

En consecuencia, una persona normalmente versada en la materia incluiría las microsíllicas de D2 en el método de la anterioridad D1, esperando con certeza lograr el producto, como la de la reivindicación 29 de la solicitud, lo cual es considerado obvio y, por lo tanto, sin altura inventiva.

Puesto que las reivindicaciones dependientes 32 y 33 no mencionan características adicionales que hagan inventiva la solicitud, se considera que tales reivindicaciones tampoco tienen nivel inventivo, ya que D2 divulga la presencia de microesferas entre el 1 y el 30% (Col. 3, líneas 30 a 54, Col. 3, línea 61 a Col. 4, línea 9) y D1 divulga que la formación es un pozo (Pág. 13, Párr. 44).

7. Conclusión

Los requisitos de Patentabilidad de la presente Solicitud están afectados así:

Item	Documento	Reivindicaciones afectadas	Requisito que afecta
D1	WO 2007/028952	16	Novedad/ Nivel inventivo
		1, 4, 8 a 15, 22, 25, 28 , 29 y 32 a 34	Nivel inventivo
D2	US 7335252	16, 18 y 21,	Novedad/ Nivel inventivo
		1, 4, 8 a 15, 22, 25, 28 , 29 y 32 a 34	Nivel inventivo

En cumplimiento del artículo 45 de la Decisión 486 de la Comisión de la Comunidad Andina, se le indica que debe dar respuesta dentro del término de sesenta (60) días contados a partir de la fecha de notificación de la presente comunicación. En caso de no dar respuesta al presente requerimiento, o si a pesar de la respuesta subsistieran los impedimentos para la concesión, se denegará la patente.

Se invita al solicitante se sirva indicar, si así lo considera, su renuncia al término faltante de sesenta (60) días para dar respuesta a este requerimiento y presentarla por escrito.

Finalmente, se le recuerda al solicitante que si como respuesta a este requerimiento llegara a modificar el capítulo reivindicatorio y éste contenga más de diez (10) reivindicaciones, no pagará la tasa de modificación voluntaria pero sí la correspondiente al pago por reivindicación adicional.

Notifíquese el presente oficio conforme a lo dispuesto en el numeral 5.2, literal e), del capítulo quinto del título primero de la Circular Única No. 10 de 2001.



JOSÉ LUIS SALAZAR LÓPEZ
Director de Nuevas Creaciones (c)

El anterior requerimiento fue notificado por fijación en lista, de fecha 2013-06-18

Elaboró: Jorge Eduardo Cortazar Gomez
Revisó: Rosa Patricia Tellez Chavarro

BENEFICIAL USES OF CEMENT KILN DUST

By:

IEEE-IAS Cement Industry Committee

Wayne S. Adaska, P.E., Director, Public Works, Portland Cement Association

Donald H. Taubert, Director, Promotion & Technical Service, Capitol Cement

Abstract:

Cement manufacturing is a critically important industry in the United States and throughout the world. In 2006, U.S. cement plants produced 99.8 million metric tons of cement. Worldwide production accounted for about 2.5 billion metric tons. As with most large manufacturing industries, by-product materials are generated. These industrial by-product and waste materials must be managed responsibly to insure a clean and safe environment. Cement kiln dust (CKD) is a significant by-product material of the cement manufacturing process. Over the past several years dramatic advances have been achieved in the management and use of cement kiln dust, thus reducing its dependency on landfill disposal.

Sustainability is the cornerstone of the cement industry, not only in the products that use cement, but also in its manufacturing process. From 1990 to 2006, the U.S. cement industry has reduced the amount of landfilled CKD 47 percent. This reduction in landfilled CKD comes despite the fact that domestic clinker production, as reported by the participants in the PCA CKD study, increased 95 percent during this same period. Overall clinker capacity in the U.S. has increased 28 percent since 1990. Many of the older, inefficient plants are being replaced by more modern plants or being renovated with new technologies to be more efficient as well as more environmentally friendly.

The majority of CKD is recycled back into the cement kiln as raw feed. In addition, new technology has allowed the use of previously landfilled CKD to be used as raw feed stock. Recycling this by-product back into the kiln not only reduces the amount of CKD to be managed outside the kiln, it also reduces the need for limestone and other raw materials, which saves natural resources and helps conserve energy.

Another principal use of CKD is for various types of commercial applications. These applications depend primarily on the chemical and physical characteristics of the CKD. The major parameters that determine CKD characteristics are the raw feed material, type of kiln operation, dust collection systems, and fuel type. Since the properties of CKD can be significantly affected by the design, operation and materials used in a cement kiln, the chemical and physical characteristics of CKD must be evaluated on an individual plant basis.

This paper will discuss the basic characteristics of CKD including current production status and regulatory requirements. Beneficial commercial uses are then presented covering a wide variety of applications including agricultural soil enhancement, base stabilizing for pavements, wastewater treatment, waste remediation, low-strength backfill and municipal landfill cover.

Introduction

Cement kiln dust is created in the kiln during the production of cement clinker. The dust is a particulate mixture of partially calcined and unreacted raw feed, clinker dust and ash, enriched with alkali sulfates, halides and other volatiles. These particulates are captured by the exhaust gases and collected in particulate matter control devices such as cyclones, baghouses and electrostatic precipitators (Figure 1).

Several factors influence the chemical and physical properties of CKD. Because plant operations differ considerably with respect to raw feed, type of operation, dust collection facility, and type of fuel used, the use of the terms typical or average CKD when comparing different plants can be misleading. The dust



Figure 1- Dust control device (Courtesy of Capitol Cement)

from each plant can vary markedly in chemical, mineralogical and physical composition (Klemm, 1993). However, to provide a general reference point, a typical dust composition as reported by the Bureau of Mines is given in Table 1.

Table 1 – Typical Composition of Cement Kiln Dust (Haynes and Kramer, 1982)

Constituent	% by weight	Constituent	% by weight
CaCO ₃	55.5	Fe ₂ O ₃	2.1
SiO ₂	13.6	KCl	1.4
CaO	8.1	MgO	1.3
K ₂ SO ₄	5.9	Na ₂ SO ₄	1.3
CaSO ₄	5.2	KF	0.4
Al ₂ O ₃	4.5	Others	0.7

At many facilities all or a major portion of the dust is recycled back into the kiln to supplement the raw feed. Other facilities market their CKD for beneficial commercial uses. For CKD not returned to the kiln system, the most common reasons are equipment limitations for handling the dust and chemical constituents in the dust that would be detrimental to the final cement product or would make the product non-compliant with applicable consensus quality standards. The fraction of the CKD that is not returned to the kiln or otherwise beneficially used is placed in landfills (Bhatty, 2004).

Cement Kiln Dust Characteristics

CKD consists primarily of calcium carbonate and silicon dioxide which is similar to the cement kiln raw feed, but the amount of alkalis, chloride and sulfate is usually considerably higher in the dust. CKD from three different types of operations: long-wet, long-dry, and alkali by-pass with precalciner were characterized for chemical and physical traits by Todres et al. (1992). CKD generated from long-wet and long-dry kilns is composed of partially calcined kiln feed fines enriched with alkali sulfates and chlorides. The dust collected from the alkali by-pass of precalciner kilns tend to be coarser, more calcined, and also concentrated with alkali volatiles. However, the alkali by-pass process contains the highest amount by weight of calcium oxide and lowest loss on ignition (LOI), both of which are key components in many beneficial applications of CKD. Table 2 provides the composition breakdown for the three different types of operation and includes a typical chemical composition for Type I portland cement for comparison.

Table 2 – Composition of CKD from Different Operation Sources (Adapted from Todres et al. 1992)

Constituent	Long-wet kiln (% by weight)	Long-dry kiln (% by weight)	Alkali by-pass from preheater/precalciner (% by weight)	Typical Type I portland cement (% by weight)
SiO ₂	15.02	9.64	15.23	20.5
Al ₂ O ₃	3.85	3.39	3.07	5.4
Fe ₂ O ₃	1.88	1.10	2.00	2.6
CaO	41.01	44.91	61.28	63.9
MgO	1.47	1.29	2.13	2.1
SO ₃	6.27	6.74	8.67	3.0
Na ₂ O	0.74	0.27	0.34	< 1
K ₂ O	2.57	2.40	2.51	< 1
Loss on Ignition (LOI)	25.78	30.24	4.48	0 – 3
Free lime (CaO)	0.85	0.52	27.18	< 2

Dust collected from gas- or oil-fired kilns contain higher proportions of soluble K₂O compared to coal-fired kilns. This is probably due to a more favorable K₂O:SO₃ molar ratio in the latter as compared to the former (Klemm, 1980).

CKD contains insignificant amounts of trace metals and therefore metal concentrations are not usually a concern for most applications. A comprehensive study evaluated the presence of trace metals in CKD from 79 plants in the United States and 10 plants in Canada using both conventional and waste derived fuels (PCA 1992). Each CKD was tested for the eight RCRA metals: arsenic, barium, cadmium, chromium, lead, mercury, selenium, and silver. The samples were also analyzed for antimony, beryllium, thallium and nickel, which are regulated under the Boiler and Industrial Furnace rule for hazardous solid wastes. Results showed that the average level of trace metals found in the CKD were significantly below the regulation limits (PCA, 1992).

The particle size of CKD is dependent upon the type of kiln operation. Muller (1977) showed that the dusts collected from dry kilns were finer than those from wet and semi-wet/semi-dry kilns. This was true for both the returned dust and the discarded dusts. Studies conducted by Todres et.al. (1992) showed that for modern cement plants equipped with alkali by-pass, the dust is relatively coarse compared to the CKD from both the wet and dry kilns. Table 3 provides a particle size distribution for three CKDs.

Table 3 – Particulate Size Distribution of Dust Samples (Todres et al. 1992)

Particulate size	long-wet kiln (% by weight)	Long-dry kiln (% by weight)	Alkali by-pass from preheater/precalciner (% by weight)
>100 µm	5.0	0.0	2.0
<45 µm	85.0	99.2	84.5
<30 µm	77.3	98.8	66.0
<7 µm	43.0	87.2	14.0
<1 µm	12.0	12.0	3.0
<0.6 µm	7.5	5.6	2.0
Median size	9.3 µm	3.0 µm	22.2 µm

According to Steuch (1992), the largest amount of dust is generated from long dry kilns in which the dust is stirred up by chains and the gas velocities are high. In contrast, in preheater kilns, feed loading is high and the resulting dust contact with kiln gases is short. Thus, the CKD generation is fairly low. Some wet

kilns produce the lowest amounts of dust, mainly because these kilns contain pebble-size dust agglomerates that are difficult to sweep away by the moving gases. Yet, the range of dust generated from these kilns does vary.

Regulatory Background

In 1976 Congress passed the Resource Conservation and Recovery Act (RCRA) (Public Law 94-580) which required EPA to develop regulations governing the identification and management of hazardous wastes. As a result, in 1978 EPA published the first set of proposed hazardous waste management standards in the Federal Register (43 FR 58946). This Federal Register notice included a proposal to exempt six categories of "special wastes" from the RCRA Subtitle C regulations until further study could be completed. Cement kiln dust was identified as one of the six special wastes.

In 1980 Congress enacted the Solid Waste Disposal Act Amendments (SWDA) (Public Law 96-482) which amended RCRA. Among the amendments, Section 3001(b) (3) (A) (i-iii) – frequently referred to as the Bevill Amendment – temporarily exempted three special wastes including CKD from hazardous waste regulation until further study could be completed. At the same time, Section 8002 (o) required EPA to study CKD and submit a Report to Congress evaluating the status of its management and potential risk to human health and the environment. EPA was also required to make a regulatory determination as to whether CKD warranted regulation under RCRA Subtitle C or some other set of regulations.

In 1993 EPA issued the Report to Congress on CKD. The report concluded that CKD generally posed little, if any, risk to human health and the environment. In 1995 EPA issued its final regulatory determination for CKD in the Federal Register (60 FR 7366). EPA determined that, though CKD may pose some risk to human health and the environment if mismanaged, it should not be regulated using overly stringent standards of RCRA's Subtitle C. Instead, EPA recommended that a more tailored set of standards be developed for managing CKD.

In 1999 EPA published "Standards for the Management of Cement Kiln Dust; Proposed Rule" (64 FR 45632). EPA's proposed approach would allow CKD to remain a non-hazardous waste provided that the specific management standards are met. CKD not managed in compliance with the standards was proposed to be a "listed waste" and would need to comply with tailored RCRA Subtitle C management standards.

The American Portland Cement Alliance (APCA)* on behalf of the cement industry submitted formal comments on the EPA proposal, opposing the use of federal authorities for CKD management. In 2000 EPA issued a Regulatory Determination addressing Fossil Fuel Combustion Wastes (FFCW), where EPA elected to retain the Bevill exclusion. Based on the logic used in the FFCW Determination, APCA filed a petition in 2001 requesting EPA withdraw the CKD proposal and reinstate the Bevill status for CKD.

In 2002 EPA published a notice of data availability (NODA) in the Federal Register (67 FR 48648). In addition to announcing the availability of new data to the public, the NODA explained that EPA was considering a new approach to CKD management whereby it would finalize the proposed CKD management standards as RCRA Subtitle D (solid waste) rule and temporarily suspend the proposed RCRA Subtitle C (hazardous waste) portion rule for 3 to 5 years to assess how CKD management practices and state regulatory programs evolve. Based upon this assessment, EPA will either formally withdraw or promulgate that portion of the 1999 proposed rule.

As of this writing no formal action has been taken on the 1999 proposed rule regarding management standards for CKD. The cement industry continues to work with EPA to resolve this issue.

Note *- The American Portland Cement Alliance (APCA) merged with the Portland Cement Association (PCA) in August 2002.

CKD Production - Past, Present, Future

The cement industry has embraced the concept of sustainability in the materials and products that use cement as well as in the manufacturing process. As a result the industry has established the Cement Manufacturing Sustainability (CMS) Program. This program, developed by PCA, addresses the Industry's commitment to sustainable development into consistent, tangible actions. The goal of the program is to balance society's need for cement products with stewardship of air, land and water, conservation of energy and natural resources, and maintenance of safe work places and communities. The centerpiece of the CMS Program is a voluntary code of conduct, which is a set of principles, performance measures, and reporting protocol, designed to guide decision making, business practices, and operating performance in a sustainable fashion (PCA, 2007).

A major element of the CMS Program is the establishment of Environmental Performance Measures. Voluntary long-term targets have been identified for each key performance measure. In the case of CKD the U.S. cement industry has adopted a year 2020 voluntary target of a 60 percent reduction (from a 1990 baseline) in the amount of cement kiln dust disposed per ton of clinker produced (PCA, 2007). Through CKD reduction efforts by PCA member companies, this goal was accomplished in 2004 as shown in Figure 2. PCA is currently developing a new CKD reduction goal.

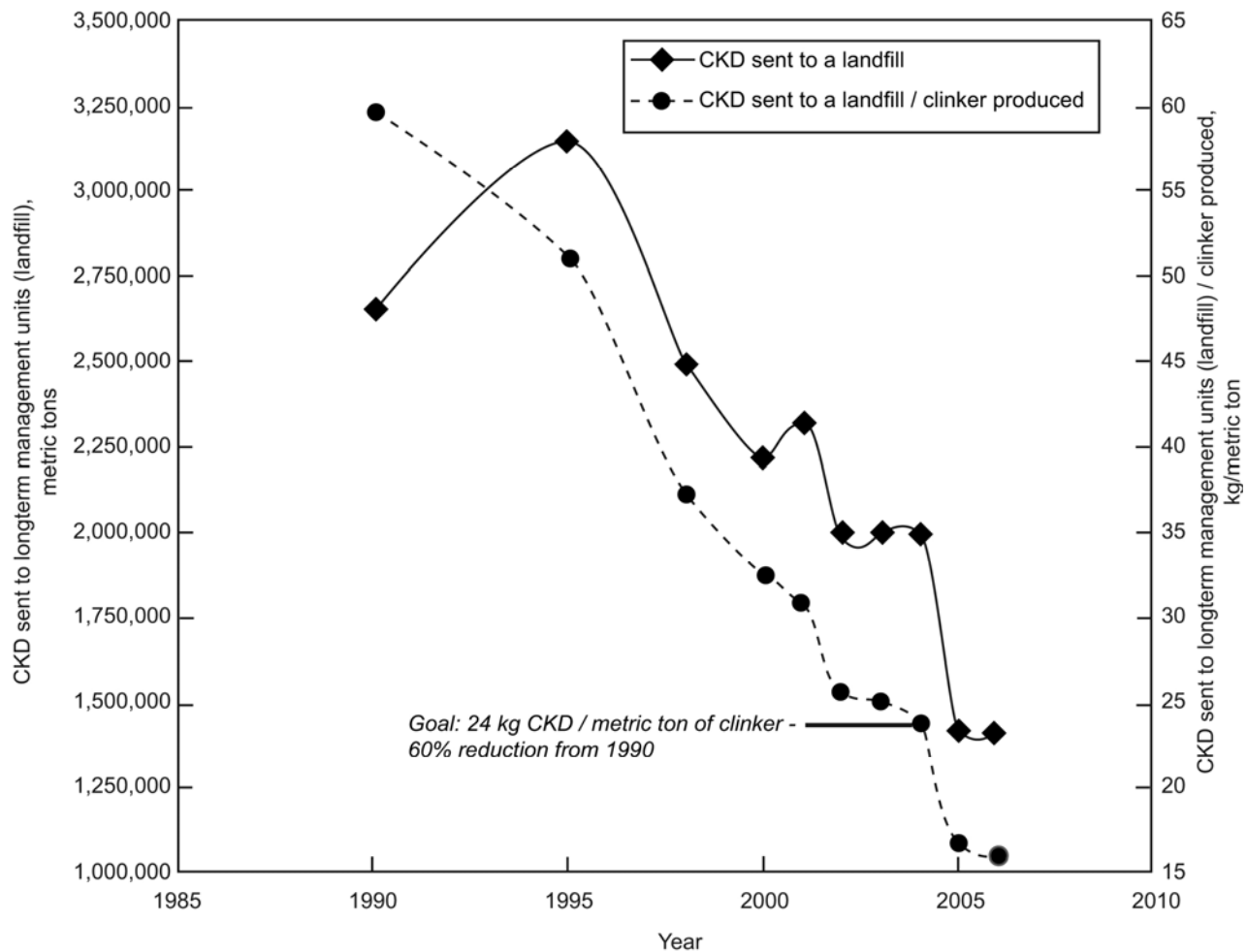


Figure 2 – Cement Kiln Dust (CKD) Disposal Rates with Reduction Goal (From PCA member company surveys)

Fewer than 20 of the 118 cement plants in the United States manage 90% of the CKD disposed on-site at cement plants. Virtually all of the disposal operations at these 20 plants are authorized – or soon will be authorized – through state solid waste programs. The plants employ management standards similar to those developed by the industry, which were largely endorsed by EPA in the 1999 proposal. Most importantly, the practice of CKD disposal continues to be phased out, as more plants are retrofitted to allow in-processing recycling. Table 4 provides a summary of management practices of CKD since 1990. The amount of CKD used for beneficial applications has increased dramatically over the 16 years the PCA members companies have been surveyed. Annual use of CKD for beneficial applications has ranged from a low of 574,800 metric tons to 1.16 million metric tons.

*Table 4 – Historical Cement Kiln Dust Production and Management**

Year	Plants responding to survey for given year	CKD beneficially reused on or off site, metric tons	CKD sent to landfill, metric tons	CKD reclaimed from landfilled, metric tons	Annual clinker production, metric tons	CKD sent to a landfill/clinker produced, kilograms / metric tons
1990	84	752,152	2,655,725	No data	44,360,364	60
1995	94	651,205	3,146,952	No data	61,729,315	51
1998	95	768,601	2,499,651	13,409	67,104,547	37
2000	92	574,803	2,223,190	79,171	68,263,086	33
2001	102	924,552	2,329,132	231,904	75,683,170	31
2002	101	664,848	1,989,680	103,223	77,636,598	26
2003	102	718,410	1,995,143	116,416	79,356,511	25
2004	102	917,968	1,993,421	69,099	83,945,430	24
2005	102	987,717	1,429,150	104,952	85,568,243	17
2006	101	1,160,011	1,403,062	261,351	86,686,834	16

Note* – From PCA member company surveys

A key performance indicator is the relationship between the amount of CKD disposed versus the quantity of clinker produced. Table 4 shows that the quantity of CKD landfilled decreased dramatically when compared to the quantity of clinker produced. It dropped from 60 kg/metric ton in 1990 to 16 kg/metric ton in 2006. This is notable given the amount of clinker produced over the same time period, increased by 95 percent. This comparison is shown graphically in Figure 3.

Cement Kiln Dust Management

Because CKD varies in physical-chemical composition between plants, the managing of dust is a plant-by-plant situation. As previously mentioned, the bulk of CKD is recycled back into the kiln system as kiln feed. The remainder of the CKD is used either for beneficial applications or landfilled. The trend in recent years indicates there has been an increase in the reuse of CKD for beneficial applications and a reduction in the amount of CKD being landfilled.

Table 5 shows the top 10 states in 2006 which beneficially reuse CKD. These ten states represent 76% of the beneficially reused CKD throughout the U.S. Of the 1.16 million metric tons of CKD removed from the cement manufacturing process in 2006, the majority of beneficial uses centered on four primary applications: stabilization/consolidation of soils, stabilization/solidification of waste materials, cement additive/blending, and mine reclamation (Table 6).

Reclaimed Previously Landfilled CKD

A recent trend at some cement manufacturing facilities is the removal or “mining” of CKD placed in landfills or other long-term management units. From the PCA CKD surveys of member companies, it was

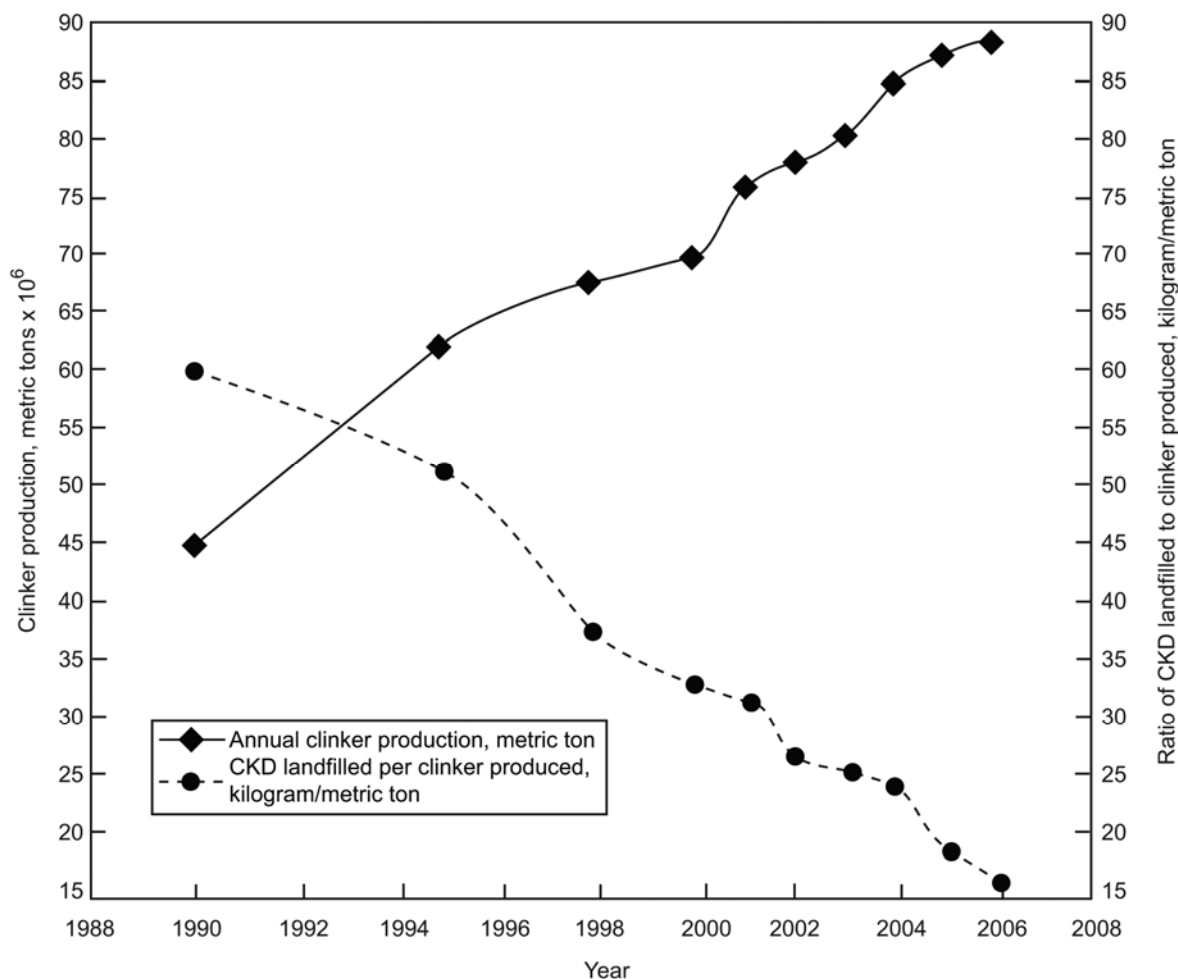


Figure 3 – Clinker Production and Ratio of CKD Landfilled/Clinker Produced (From PCA member company surveys)

learned that the amount of CKD removed from onsite landfills has grown from just over 13,400 metric tons in 1998 to more than 261,000 metric tons in 2006 (Table 4). Because CKD is very similar to the raw materials entering the kiln system and may contain partially processed feed or final product, the CKD becomes more valuable as energy and other manufacturing costs rise. Through the addition of equipment for the return of dust to the kiln (dust insufflation equipment or dust scoops), long kilns can return a portion or all of their dust.

Table 5 – States with the Highest Amount of CKD Used for Beneficial Applications*

State	Quantity of CKD beneficially reused, metric tons	State	Quantity of CKD beneficially reused, metric tons
Oklahoma	154,477	Indiana	82,325
Texas	144,043	California	66,801
Pennsylvania	102,760	Arkansas	61,990
Ohio	86,453	Maryland	50,562
Illinois	85,330	Missouri	48,250

Note* – From PCA member company survey for 2006

*Table 6 – Beneficial Uses of Cement Kiln Removed from the Cement Manufacturing Process**

Uses of CKD	Quantity of CKD beneficially reused, metric tons
Soil / Clay Stabilization / Consolidation	533,365
Waste Stabilization / Solidification	213,675
Cement Additive / Blending	183,228
Mine Reclamation	152,756
Agricultural Soil Amendment	33,546
Sanitary Landfill Liner / Cover Material	15,042
Wastewater Neutralization / Stabilization	12,302
Pavement Manufacturing	12,066
Concrete Products	374
Beneficial Use Not Provided	3,657
Total	1,160,011

Note* – From PCA member company survey for 2006

Cement plants that convert an existing long kiln into a semi-dry, preheater, or preheater/precalciner process or add such a kiln system to their facility may choose to remove CKD from existing landfills to augment the raw materials and CKD internally recycled to the manufacturing process. To do such “mining” will be a site-specific decision dependent on the impact to final product, plant operations, energy use, and economic benefits.

A Thomaston, Maine cement producing plant utilizes recovery scrubber technology to manage its CKD, recycles not only all the CKD it generates, but also consumes CKD from its on-site stockpile of dust generated during 100 years of operation. Material from this pile is being mined and reintroduced to the kiln at a rate of approximately 90 to 270 metric tons per day.

In 2006, PCA member companies were asked to provide details on the use of CKD reclaimed from landfills or other long-term management units. The reported beneficial uses of the reclaimed CKD are summarized in Table 7. Nearly half of the CKD was returned to the kiln system for the manufacture of clinker. Other beneficial uses included the stabilization/solidification of waste materials, agricultural soil amendment, and stabilization/consolidation of soils. Because of the wide variation in the chemical and physical composition of the landfilled CKD, CKD removed from existing landfills for any beneficial use would be a site-specific decision.

*Table 7 – Beneficial Uses of CKD Reclaimed from Landfills**

Uses of CKD	Quantity of CKD beneficially reused, metric tons
Returned to Kiln	114,935
Waste Stabilization / Solidification	91,982
Agricultural Soil Amendment	27,745
Soil / Clay Stabilization / Consolidation	21,321
Wastewater Neutralization / Stabilization	2,901
Cement Additive / Blending	2,331
Pavement Manufacturing	137
Total Reclaimed from Landfills	261,352

Note* – From PCA member company survey for 2006

CKD for Blended Cements

The use of CKD as an addition to portland cement has been evaluated by a number of researchers. A summary of some examples can be found in Detweiler et al. (1996). M. S. Y. Bhatti (1983, 1984a-c, and 1986) published a series of reports on the use of CKD blended with portland cement as well as fly ash and ground granulated blast furnace slag. The studies found that cements containing only CKD had reduced workability, setting times, and strength. The loss of strength was attributed to alkalies in the dust. It is believed that the use of fly ash with CKD diluted the alkalies and thus improved the strength. Addition of slag to a cement-CKD blend generally decreased workability, but produced higher strengths than blends containing no slag. It was found that blended cement with high sulfate produced the greatest strength, and that the impact of the alkalies in the dust could be negated by the fly ash and/or slag. Overall, the ratios of alkali, chlorides, and sulfates in the dust are important in determining the properties of the blended cement.

Ravindrarajah (1982) reported that kiln dust could be used in masonry and concrete blocks without loss of strength or workability. His study showed that up to 15% of the portland cement could be replaced with CKD. If higher percentages of dust were used, the setting was retarded, workability was reduced, and water demand was increased.

Daugherty and Funnell (1983) reported that the use of up to ten percent interground CKD did not have any adverse effects on the setting time, soundness or shrinkage of the final portland cement concrete. However, the strength results varied, most likely attributed to the changing dust composition.

Abo-El-Enein et al. (1994) studied the mechanical properties of blended cements using by-pass dusts. The initial and final setting times of cement pastes were decreased due to the high free lime content in the CKD. Blended cements with up to 15% kiln dust had increased compressive strengths and accelerated hydration. Compressive strengths decreased when more than 15% of the portland cement was replaced with CKD.

Soil Stabilization

The value of CKD is not limited to its use as a raw material for return to the cement kiln or as an additive in a blended portland cement. CKD is also used in a variety of other applications as-is or in combination with other additives. Methods for determining and evaluating characteristics of CKD suitable for various applications are given in ASTM D5050 *Standard Guide for Commercial Use of Lime Kiln Dusts and Portland Cement Kiln Dusts*.

As indicated in Table 6, more than half million metric tons of CKD was used for soil stabilization. Because of the free lime content and ability to enhance the effectiveness of other stabilizers like fly ash, CKD has been used extensively as a binder in soil stabilized base and subbase pavement applications (Figure 4).

Sayah (1993) and Zaman et al. (1992) have demonstrated the effectiveness of CKD in stabilizing highly expansive clay soils. Their data showed similarities to those for portland cement, fly ash, and lime for stabilizing expansive soils. Miller et al. (1980) used CKD and fly ash in stabilized base courses in road construction in the form of a pozzolanic non-cement concrete with limestone as an aggregate. Such mixes were also found to have autogenous healing characteristics. McCoy and Kriner (1971) reported a wide range of tests conducted on kiln dust compositions for soil stabilization. The use of CKD in stabilization of clays has been shown to improve the unconfined compressive strength and reduce the plasticity index using dust with low LOI. On the other hand, adding CKD with high LOI resulted in relatively lower unconfined compressive strengths and higher plasticity indices (Bhatti et al., 1996).



Figure 4 – Constructing a pavement base using CKD (Courtesy of Lafarge North America)

Miller and Zaman (2000) indicated that CKD can be used as an alternative to quick lime for subgrade stabilization in highway construction. The laboratory and field test data showed that CKD was more effective than quicklime for stabilizing soil. Additional laboratory tests showed that the influence of CKD and lime on the plasticity index of soils was similar and that both additives imparted some resistance to freeze-thaw and wet-dry cycles. In addition, the tests showed that the LOI content was an important factor in the effectiveness of the CKD. High LOI implies a higher percentage of bound water within its chemical structure and less CaO available to react. Conclusions were that treatment with CKD can be cost-effective and that it requires less construction time than treatment with quicklime.

The Kansas Department of Transportation (KDOT) preformed cyclic wet-dry durability tests on CKD and determined that CKD preformed similar to other stabilizing additives in regard to the number of cycles survived (KDOT, 2004). The Oklahoma Department of Transportation (ODOT) conducted tests on CKD to determine swell potential. Results showed negligible swelling tendencies. The results also found that shale treated with both quick lime and CKD preformed similarly throughout the curing process. However after 14 days of curing the quick lime proved much less effective than CKD (ODOT, 2003). ODOT has incorporated approved procedures for using CKD (ODOT, 2004) as well as mix design procedures for soil stabilization and soil modification (ODOT, 2006a-b).

The U.S. Department of Transportation and the U.S. Department of Energy tested the effectiveness of substituting CKD for hydrated lime in lime-fly ash-aggregate road base systems. CKD was found to perform well in pozzolanic road base compositions involving some form of lime-fly ash stabilization. CKD generally yielded mixes with high resistance to freezing and thawing and some mixes developed early strength, possibly extending the normal cut-off dates for late season construction. The study found that, with few exceptions, fresh CKD worked with nearly any fly ash to produce strengths high or even higher than those observed with commercial hydrated lime and fly ash, although larger CKD quantities were required compared to normal hydrated lime to achieve the same strength. The study also found that aged CKD from stockpiles had a lower free lime content and resultant poor reactivity. In addition, CKD from dry process plants tended to produce the highest strength. Total dusts containing both fine and coarse CKD were better than separated CKD. The study concluded that, owing to its free lime content, CKD may be used in lieu of hydrated lime as a pozzolanic road base material (Valley Forge Laboratories, Inc., 1982).

Waste Stabilization/Solidification

CKD use has also been reported in a number of solidification/stabilization projects, primarily in remedial actions, and central hazardous waste management facilities. The absorptive quality of the dust, along with its high alkaline nature makes it very effective for waste treatment. Connor (1990) and others (1992) went into great detail on the chemistry and applicability of CKD in the stabilization of soils and sludges, including several case studies. A paper by MacKay and Emery (1992) describes the stabilization of contaminated soils and sludges in which CKD is used in conjunction with other cementitious products such as slag cement, lime kiln dust, fly ash, hydrated lime, and portland cement.

Several uses of CKD for the stabilization/solidification of specific wastes have been suggested over the last several decades. Coccozza (1977) and Holley (1992) patented processes in which flue gas desulfurization residues are treated to produce stable, leach-resistant solids. The CKD-fly ash process developed by Nicholson (1982), is applicable to sewage sludge solidification, but appears to be equally appropriate for other wastes. Ader et al. (1989) proposed a method for the stabilization of mercury-containing waste while Kigel et al. (1994) developed a chromium ore waste treatment utilizing CKD. Funderburk (1990) suggested a method of solidifying and immobilizing hazardous waste in an organic matrix using CKD as one of the components, and Weszely (1996) proposed a general solidification process of hazardous waste.

At the Port of Richmond on San Francisco Bay, CKD was used as part of a cost-effective sediment remediation program. The CKD was used to turn contaminated sediment dredged from a marsh and shoreline into an engineered fill. Approximately 5,100 cubic meters of treated material were reused as a structural subbase material for a paved parking lot (Bourne, 2007).

The final process in handling hazardous wastes is the responsibility of the treatment, storage and disposal facility (TSDF). The regulations pertaining to TSDFs are more stringent than those that apply to generators, transporters or municipal landfill operators. US Ecology Texas (USET), a division of American Ecology is a licensed TSDF permitted under Subtitle C of RCRA. The USET facility is located in Robstown, TX near Corpus Christi and includes a 97 hectare active waste site. The facility, which began operations in 1973, treats and disposes of RCRA, PCB remediation waste, and low-concentration NRC-exempt radioactive waste. USET is capable of treating a wide variety of organic and inorganic wastes, either liquid or solid. The use of CKD plays an integral part in the treatment. Table 8 provides a partial list of wastes that can be treated with CKD.

Table 8 – Partial list of Hazardous Wastes Treated with CKD (Source USET)

Aqueous wastes	Metal solids	Plating sludge	Organic & Inorganic liquids
Spent acids	Petroleum solids	Drilling mud	Organic paint/ink/lacquer
Spent caustics	Adhesives/epoxies	Catalyst wastes	Ethylene glycol antifreeze
Waste oils	Incinerator residues	Resins/tar sludge	Leachate contaminated wastes
Brine solutions	WWT sludge	Contaminated soil	Hazard sandblasting wastes

The process in determining the appropriate treatment begins by first evaluating the materials through an on-site laboratory using profile information and shipment samples to determine what compounds/toxins are present, and what would be the proper mix design to solidify or treat the material. Once this procedure is established; treatment starts. The material to be treated is placed into a 92 cubic meter treatment tank; CKD is added and homogenized with a backhoe type mixer (Figure 5). CKD has proved to be effective in reducing pH of acidic materials. It has also been shown to be effective in treating listed solid and liquid hazardous wastes, refinery and drilling industry wastes.

The Texas Commission on Environmental Quality requires a minimum unconfined compressive strength of 345 kPa be achieved prior to disposal. This criterion can be met with as little as 10% CKD, but may require up to 200% addition. The CKD comes from a San Antonio based cement plant and contains a relatively high CaO content (60.9% by weight) and low LOI (2.2% by weight) making it well suited for this



Figure 5 – Mixing wastes in treatment tank (Courtesy of USET)

type of application. After the material is processed, it is stored for verification of treatment and approved for disposal. Subsequently, it is placed into a landfill and covered.

According to Kenneth Knibbs, General Manager of USET facility, “CKD works better than other granular or dust type materials. It may take a little more, but it’s so much easier to use. The CKD can be handled with end-loaders, it’s not extremely dusty and it’s easy to mix.”

Sanitary Liner and Cover Material

Studies have been carried out to use CKD as a watertight barrier (liner) for sanitary landfill sites (Ballivy et al., 1992). The dust could be consolidated and stabilized when used in conjunction with varying amounts of Class C fly ash and silica fume. The mixes had a water to dry-solid ratio of 0.4 and were cured at 100% relative humidity for 10 days after demolding. After consolidation the mixes showed permeability lower than the standard 10^{-7} cm/sec. When tested as liners, these mixes exhibited a good capacity for absorbing heavy metals.

Cement kiln dust was used successfully as a cover material instead of clay at a sanitary landfill located at a California cement plant (Crosby et al., 2000). In the early 1900s, cement plant employees began disposing of household waste at the company’s on-site landfill. This practice continued until the mid-1980s when landfill disposal was limited to construction debris. In the 1990s, all waste disposal was stopped, and the regulatory closure process began. From detailed geotechnical testing, the State of California determined that compacted CKD would be an acceptable landfill cover material. CKD was also used as a fill material to protect the landfill from erosion from future storm events. Also, the cost of the CKD was calculated as only 20% of what was estimated for alternative cover and fill materials.

Hansen (1996) developed a synthetic waste pile cover material based on a mixture of fibers (paper, wood, and/or plastic) and a cementitious material such as CKD. A slurry of this material would be applied to a waste pile and allowed to harden to minimize water infiltration, fugitive dust releases, odor, and animal intrusion. An example of a spray-applied coating used for landfill daily cover is shown in Figure 6.



Figure 6 – Spray applied coating used for landfill daily cover (Courtesy of Landfill Services Corp)

Mine Reclamation

The U.S. Bureau of Mines study (Haynes and Kramer, 1982) documented the use of CKD as partial hydraulic filler for backfilling coal mine shafts and tunnels. Because of its fine particle size and high alkali contents, CKD is also being premixed to neutralize acidic media and effluent from mining and mineral processing industries. For instance, CKD was used to neutralize a chemical pond containing acidic sulfates. The attempts were only partially successful because the particular CKD used was very coarse (Klemm, 1980). Nehdi and Chan (2007) reported on the stabilization of sulfuric mine tailings to prevent metal release and acid drainage.

The dust also has the potential to replace fly ash for controlling the spread of fires in coal mines. CKD has also been used as a binder in pelletizing iron ore fines for recycling in steel making. It has also found applications as coagulant for dewatering of waste sludge from tin rolling mills (Klemm, 1980).

Agricultural Amendment

Because of the high lime and potassium concentrations, CKD is used as a soil amendment or fertilizer in many parts of the world. The acid neutralizing capacity of the lime in CKD counteracts the acidic soils that result from years of farming. Neutral soils are a better growing environment for crops and also enhance herbicide effectiveness. The dust may provide potassium and trace metals that are also depleted from agricultural soils due to plant withdrawal requirements. The following describe some of the work that has been completed on this subject within the U.S.

For agricultural uses of CKD in the U.S. before 1975, Davis and Hook (1975) completed a survey of dust applications in their report for the USEPA. They found that kiln dust was suited to replace liming agents and potassium fertilizers. Baker et al. (1975) developed nonputrescible soil-like products for general agricultural applications by combining CKD with sewage sludge before vacuum filtering. Risser et al. (1981) produced a lime-potash soil additive composed of 35% CaO, 6% MgO, 5% K₂O, and 4% SO₃ from CKD having a controlled composition. Taylor (1987) also reported the usefulness of CKD as a substitute for lime and fertilizer elements. Since the quality of CKD varies with each cement plant, however, the nutrient value may also change. In Australia, Dan et al. (1989) found that CKD increased the crop yield equally well as crushed limestone. Fraiman et al. (1991) recommended the use of bypass dust containing high levels of K₂O, SO₃, and Cl, in fertilizer applications. Because potassium is the most valuable fertilizer

element contained in the dust and the least desirable element for recycling, CKD with high potassium contents could be adequately utilized as a fertilizer. It should be noted that nutrients such as nitrogen and phosphorus are still required from other sources regardless of whether limestone or CKD is used on agricultural soils.

Because the placement of a fine dust, such as CKD, on agricultural lands is difficult, it has been suggested that granules or agglomerates of dust should be made (Kachinski, 1983; Wommack et al., 2001). The larger particles help to limit fugitive releases of dust while transporting, handling, and placing the CKD. Conversely, care must be taken so that the granules are not so rigid that rain and other natural processes cannot dissolve or break down the particles to release the beneficial constituents of the dust.

One of the concerns with using CKD as a fertilizer or soil amendment is the level of trace metals it may contain. The effect of those metals on the food chain through possible extraction by soil and subsequent movement into vegetation should be determined before such applications are to be considered. However, in a specific study on the use of CKD as a fertilizer in Iowa, Preston (1993) demonstrated that trace metals in CKD were well below the permissible levels for land application.

The USEPA (1999b) studied metals and other constituents of fertilizers including CKD. Their findings showed that the metals content of various fertilizers ranged over several orders of magnitude but did not provide any specific recommendations on the use of CKD on agricultural lands.

Kanare (1999) completed a study comparing CKD to soils, agricultural limestones (aglime), and sewage sludges. He found that sludges generally have the highest levels of chromium, lead, mercury, nickel, and silver compared to CKD, aglime, and North American soils. The highest levels of thallium and selenium are found in CKD. Other elements of interest are present in these materials at non-detectable or comparable concentrations.

Controlled Low-Strength Material (CLSM)

Controlled low-strength material (CLSM) is a self-compacted, cementitious material used primarily as a replacement for compacted soil fill. The American Concrete Institute (ACI) further defines CLSM as a material having a maximum compressive strength of 8.3 MPa. Often the ability to excavate CLSM at a later date is an important factor. In these cases, in many cases compressive strengths in the range of 0.7 to 1.4 MPa are specified. Because of the low strength requirements, CKD maybe well suited as a replacement or supplementary material to portland cement and fly ash.

Ramchairitar et al. (2003) studied different replacement ratios to determine comparable properties with CLSM mixtures using cement only. His studies indicated that slump and bleeding decreased with increasing CKD content, while compressive strength increased with increasing CKD content. He concluded that replacing the 25 kg/m³ of cement in the control mix with 50 kg/m³ of CKD gave the most optimum results.

Katz and Kovler (2004) investigated the effects of various by-product materials including CKD in CLSM. Fly ash mixtures showed greater bleeding than mixtures containing CKD. Fly ash mixtures had bleeding in excess of 3%, while CKD mixture reached a maximum of around 1%. The setting time of CKD mixtures was longer than those mixtures containing fly ash. Compressive strengths of CKD mixtures were less than corresponding mixtures containing equal amounts of fly ash.

Williams (2005) studied the effects of four distinctly different CKDs on the properties of CLSM. The four CKDs covered the range of high and low calcium oxide (CaO) and high and low loss on ignition (LOI). Results indicated that mixtures produced with CKD but no fly ash always set and hardened more slowly. Without fly ash, the mixtures containing CKD with high LOI never hardened. Compressive strengths of the mixtures varied considerably. In general the compressive strengths decreased with increasing CKD content and decreasing fly ash content. Of the CKD properties considered (CaO content and LOI); the LOI had the most significant impact on the hardened properties of CLSM. Mixtures containing low LOI

(<10%), regardless of content, had compressive strengths from 1.0 MPa to 10.3 MPa at 56 days. CKD having high LOI (>20%) could only obtain strength if fly ash or cement was added. Mixtures containing high LOI CKD, regardless of content, had compressive strengths less than 1.4 MPa up to 90 days. However, a small amount of cement vastly increased the strength.

Miscellaneous Applications

CKD has been used as a substitute for lime in stabilizing wastewater streams. This is possible primarily because of the high neutralizing potential of the CKD (high CaCO_3 , and CaO) and fine particle size distribution, having Blaine finenesses often greater than 800 m^2/kg . Up to a 35% addition of CKD has satisfactorily met the specified pathogen control level in sewage sludge. High pH, an exothermic reaction, and the resulting accelerated drying when CKD was added were the factors mainly responsible for the pasteurizing effects on municipal wastewater sludge (Nicholson, 1988a and 1988b; Burnham, 1987; Nicholson and Burnham, 1988). Canadian study found that CKD could be used instead of caustic soda in the treatment of wastewater from a pulp and paper factory (Smith and Campbell, 2000).

Hydrated CKD has also been successfully evaluated as an anti-stripping agent in hot-mix asphaltic concrete (Klemm, 1993). Preliminary tests on replacing up to 3% hydrated lime by the hydrated CKD have shown favorable results. CKD has been used as inorganic filler in bituminous paving and asphaltic roofing. Kiln dust has also been used as filler for asphaltic insulating board sound-deadening materials (Davis and Hooks, 1975).

Cement kiln dust has also been used as a partial replacement for soda in the production of glass where color and high chemical stability are not essential considerations. High alkalies in CKD increase the rate of sulfate decomposition that is the main cause of foaming in glass baths (Emer, 1969). A soda-kiln-dust glass has many similarities to the conventional soda-lime glass. Fraiman et al. (1991) have also recommended the use of bypass dust in glass making.

In some Eastern European countries, kiln dust has been successfully incorporated into cementing compositions for gas and oil wells. The kiln dust appears to improve slurry pumpability and also functions as a fluid-loss additive. CKD also sufficiently retarded oil well cement slurries for use at temperatures up to 100°C, without additional retarders.

Conclusions

Cement kiln dust (CKD) is a significant by-product material of the cement manufacturing process. Over the past several years dramatic advances have been achieved in the management and use of cement kiln dust, thus reducing its dependency on landfill disposal.

From 1990 to 2006, the U.S. cement industry has reduced by 47 percent the amount of CKD landfilled. This reduction in landfilled CKD comes despite the fact that domestic clinker production, as reported by the participants in the PCA CKD study, increased 95% during this same period. Overall clinker capacity in the U.S. has increased 28 percent since 1990.

The majority of CKD is recycled back into the cement kiln as raw feed. In addition, new technology has allowed the use of previously landfilled CKD to be use as raw feed stock. Recycling this by-product back into the kiln not only reduces the amount of CKD to be managed outside the kiln, it also reduces the need for limestone and other raw materials, which saves natural resources and helps conserve energy.

The value of CKD is not limited to its use as a raw material for return to a portland cement kiln. There are many other beneficial uses of CKD including base stabilizer for pavements, solidifier and stabilizer for contaminated wastes, agricultural soil enhancement, low-strength backfill material and municipal daily landfill cover.

Studies have shown that CKD can be used alone, but often is more effective when used in combination with other cementitious materials including portland cement, fly ash and slag. CKD containing high CaO content and low loss on ignition (LOI) performs best for most applications. High LOI dusts contain a higher percentage of bound water within its chemical structure and less CaO is available to react. The high LOI can also interfere with the hydration process.

Several processing factors influence the chemical and physical properties of CKD. Because plant operations differ considerably with respect to raw feed, type of operation, dust collection facility, and type of fuel used, CKD from each plant can vary markedly in chemical, mineralogical and physical composition. Therefore it is important to thoroughly test CKD for any proposed application prior to use.

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