

[SS 1] ..fi epodoc

 Database: EPODOC

[EPODOC: SS 1] ELECTROMAGNETIC and TOROIDAL and IMPULSOR

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[SS 2] ELECTROMAGNETIC and TOROIDAL and IMPULSORreactor

Results in EPODOC 0

EPODOC: term 'IMPULSORREACTOR' not found in index 'BI'. WARNING(1)

[SS 3] ELECTROMAGNETIC and TOROIDAL

Results in EPODOC 671

[SS 4] ss3 and reactor

Results in EPODOC 5

[SS 5] ..li



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PN - [CN204119065U](#) U 20150121

PR - CN20142249462U 20140516

AP - CN20142249462U 20140516

DT - I

CCA - [Y02T10/7241](#)

PA - NORTH CHINA INST SCI & TECH

TI - **SS3** electric locomotive auxiliary converter phase control rectifier circuit

AB - The utility model provides an **SS3** electric locomotive auxiliary converter phase control rectifier circuit comprising a rectifier bridge, a smoothing **reactor** L and a bus support capacitor Cd; the rectifier bridge comprises two thyristors, two diodes and another two diodes connected in parallel; an output end of the rectifier bridge is connected in series with the smoothing **reactor** L, and connected with an outer load through the bus support capacitor Cd; a first phase of an output voltage of a main transformer auxiliary winding is connected on a connecting line between the two thyristors, and a second phase of the output voltage of the main transformer auxiliary winding is connected on a connecting line between the two diodes. The **SS3** electric locomotive auxiliary converter phase control rectifier circuit is simple in reconstruction and setting, and can realize fast conversion between a split-phase motor of a reconstructed **SS3** locomotive and a previous converter.

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PN - [JPS5960619](#) A 19840406

PNFP - JPH0152993B B2 19891110

PR - JP19820171820 19820930

AP - JP19820171820 19820930

DT - I

CCI - [G05F1/70](#)

FI - G05F1/70&L; G05F1/70&M; H02J3/18&C; H02J3/18&142; H02M5/27&G

FT - 5G066/FA07; 5G066/FB12; 5G066/GA02; 5G066/GC01; 5H420/BB02; 5H420/BB12; 5H420/BB16; 5H420/BB18; 5H420/CC05; 5H420/CC09; 5H420/DD04; 5H420/DD06; 5H420/EA03; 5H420/EB05; 5H420/EB26; 5H420/EB39; 5H420/FF03; 5H420/FF04; 5H420/FF17; 5H420/FF19; 5H420/FF22; 5H420/FF23; 5H420/FF26; 5H420/GG04; 5H420/HJ08; 5H420/HJ09; 5H420/LL04; 5H750/AA02; 5H750/AA04; 5H750/BA01; 5H750/BA06; 5H750/BB02; 5H750/BB25; 5H750/CC03; 5H750/CC11; 5H750/CC14; 5H750/CC16; 5H750/CC20; 5H750/DD05; 5H750/EE01; 5H750/FF02; 5H750/FF05; 5H750/JJ03

PA - (A)
TOSHIBA KK

TI - (A)
ELECTRIC POWER ADJUSTING DEVICE

AB - (A)
PURPOSE:To obtain an electric power adjusting device which can excute the balancing of a polyphase power and compensation of a reactive power with separately excited converters, whose number is reduced to half from conventional devices, by providing a high-frequency reactive power source composed of a condenser or a condenser and AC **reactor**, and others. CONSTITUTION:A high-frequency reactive source composed of a condenser or a condenser and AC **reactor**, and others are provided. For example, compensating currents Icu, Icv, and Icw are supplied to a 3-phase AC power source through AC reactors AL1, AL2, and AL3 and a power transformer TRs from the center tap of the DC reactors L1, L2, and L3 of a circulating current type cyclo converter composed of separately excited converters SS1, SS2, and **SS3** and DC reactors L1, L2, and L3. The AC-side terminals of the separately excited converters SS1, SS2, and **SS3** are connected to a phase advance capacitor CAP which is the high-frequency reactive power source. The circulating current of the cyclo converter flows so that the advanced reactive power of the phase advance capacitor CAP and the delayed reactive power of the cyclo converter are faded out by each other.

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PN - [JPS5860328](#) A 19830409

PNFP - JPH0221220B B2 19900514

PR - JP19810158692 19811007

AP - JP19810158692 19811007

DT - I

CT - || STSE (A)

[JPS5858621](#) A 19830407 [] (TOKYO SHIBAURA ELECTRIC CO)

CCI - [G05F1/70](#)
FI - G05F1/70&H; G05F1/70&M; H02M5/27&G; H02M7/515&E
FT - 5H007/AA00; 5H420/BB02; 5H420/BB11; 5H420/BB13; 5H420/BB16; 5H420/CC05; 5H420/CC09; 5H420/DD04; 5H420/DD06; 5H420/EA03; 5H420/EB05; 5H420/EB38; 5H420/FF04; 5H420/FF07; 5H420/FF22; 5H420/FF25; 5H420/FF26; 5H750/AA04; 5H750/AA10; 5H750/BA01; 5H750/BA06; 5H750/BB02; 5H750/BB25; 5H750/CC03; 5H750/CC11; 5H750/CC14; 5H750/CC20; 5H750/DD05; 5H750/FF02; 5H750/FF05; 5H750/FF09
PA - (A)
TOKYO SHIBAURA ELECTRIC CO
TI - (A)
REACTIVE POWER CONTROL TYPE CYCLO CONVERTER DEVICE
AB - (A)
PURPOSE:To remove the reactive power variation of a receiving end and keep a fundamental wave power factor "1" by composing the titled device of three AC/DC power converters and a **reactor** with an intermediate tap, making one- way circulating current flow into the DC side and controlling the current. CONSTITUTION:A reactive power operator VAR connected to an 3phi AC power source operates its reactive power Q. The command value Q* of reactive power is ordinarily set to "0" and a comparator CQ outputs the deviation epsilonQ between the operated value and the command value. A controlling and compensating circuit H(S) generates an output I0* to set up the deviation epsilonQ to "0" and the output I0* is used as a the command value of circulating current I0. The deviation epsilon0 between the I0* and I0 is found by a comparator C0, amplified by an amplifier K0 and applied to adders A1-A3. These adders A1-A3 add the deviation epsilon0 to respective phase current deviation and the added values are supplied to converters SS1-SS3 through phase control circuits PH1-PH3, so that current I0 flows through DC reactors L1-L3. The current I0 increases the invalid component of the whole input current ICC of a converter. Consequently the fundamental wave power factor of an receiving end can be kept "1" by controlling the current I0.

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PN - [JPH02261057](#) A 19901023
PNFP - JPH0691749B B2 19941114
PR - JP19890078409 19890331
AP - JP19890078409 19890331
DT - I
FI - H02M5/27&E; H02M5/27&G; H02M5/27&H
FT - 5H750/AA04; 5H750/AA10; 5H750/BA01; 5H750/BA06; 5H750/BB02; 5H750/BB27; 5H750/BB30; 5H750/CC03; 5H750/CC11; 5H750/CC16; 5H750/DD05; 5H750/DD25; 5H750/EE03; 5H750/FF02; 5H750/FF05
PA - (A)
TOSHIBA CORP
TI - (A)
DELTA CONNECTION CYCLOCONVERTER

AB - (A)
 PURPOSE: To eliminate the voltage drop of a DC **reactor** and impress the output voltage of a converter on a load terminal as it is by winding the coils of 3 sets of DC reactors around a same core to connect them magnetically. CONSTITUTION: The title device is provided with the electric wire passage BUS of 3-phase AC power source, a power source transformer TR, separately excited converters SS1-**SS3**, DC reactors L1-L3 wound around a same core and an AC motor M. The boils of three sets of the DC reactors L1-L3 are wound around the same core whereby the self inductance of one winding is equalized to the mutual inductance of the other two windings and affections due to the output currents I1-I3 of three sets of converters SS1-**SS3** are equalized. According to this method, the output voltage of the converters SS1-**SS3** may be designed without considering the voltage drop of the AC reactors L1-L3 and an AC voltage may be reduced by an amount corresponding to the voltage drop.

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PN - [JPS56101306](#) A 19810813
 PNFP - JPS6032407B B2 19850727
 PR - JP19800003382 19800116
 AP - JP19800003382 19800116
 DT - I
 FI - B60L13/02&V; B60L13/03&V; H02P25/06; H02P25/064; H02P7/00&101B
 FT - 5H113/AA01; 5H113/AA05; 5H113/AA06; 5H113/CC04; 5H113/CC08; 5H113/FF01; 5H113/GG02; 5H113/GG08; 5H113/GG12; 5H113/GG13; 5H113/GG14; 5H113/HH01; 5H113/HH04; 5H113/HH08; 5H113/HH11; 5H113/HH13; 5H113/HH14; 5H113/HH17; 5H113/HH28; 5H113/HH29; 5H540/BA03; 5H540/BB05; 5H540/BB09; 5H540/EE08; 5H540/FC02; 5H540/FC03; 5H540/FC04
 PA - (A)
 JAPAN NATIONAL RAILWAY; TOKYO SHIBAURA ELECTRIC CO
 TI - (A)
 DRIVING DEVICE FOR LINEAR MOTOR
 AB - (A)
 PURPOSE: To eliminate the distortion of the waveform of a load current in the linear motor by so controlling the circulating current of a cyclo-converter that the lagging reactive current of the cyclo-converter and the leading reactive current of a phase advance capacitor cancel one another. CONSTITUTION: The reactive power Q of a power receiving terminal including the phase advance capacitor C is calculated by a reactive power arithmetic circuit VAR, and a deviation epsilon1 between the reactive power Q and an instruction value Q* is produced through a control compensating circuit H(s) as a command value I0* for the circulating current. An adder A1 subtract the current I00 flowing through the intermediate DC **reactor** L00 of the cyclo-converter by the load current IU, and divides the deviation by 2 to thus detect the circulating current I0. After the deviation epsilon2 between the instruction value I0* and the circulating current I0 is added to the current deviation signal epsilon3, the sum is applied to the phase control circuits PH1-PH4 of positive and negative group converters SS1, SS4 and SS2, **SS3**.

