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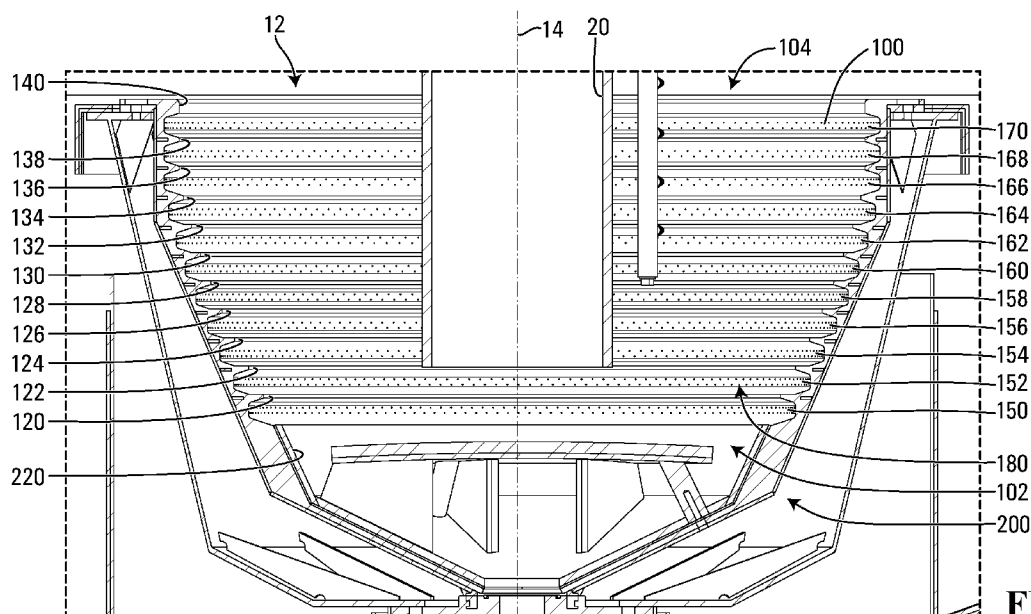
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(57) Abstract: An apparatus for facilitating particle separation by density includes a separator having an inner surface surrounding a rotation axis and defining a particle path from an input end to an axially spaced output end. The inner surface includes a plurality of axially spaced dividers having respective inner positions, defining at least in part respective axially spaced retainers for collecting particles during rotation of the separator. The retainers each include at least one fluid inlet for fluidizing particles in the retainer during operation. The dividers include a first pair of adjacent dividers and a second pair of adjacent dividers, the first pair nearer the input end than the second pair, wherein a first divider slope of the first pair is greater than a second divider slope of the second pair and wherein each of the first and second divider slopes is zero or positive. Other systems, apparatuses and methods are disclosed.

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PARTICLE SEPARATION BY DENSITY

CROSS REFERENCES

5 This application claims the benefit of U.S. Provisional Application No. 63/013,289 entitled "PARTICLE SEPARATION BY DENSITY", filed on April 21, 2020, which is hereby incorporated by reference herein in its entirety.

BACKGROUND

1. Field

10 Embodiments of this present disclosure relate to particle separation and more particularly to particle separation by density.

2. Description of Related Art

15 Some systems for separating particles by density may cause particles to flow across riffles or dividers, such that higher density particles are stopped by the dividers and lower density particles pass over the dividers. The systems may include respective retainers or recesses for collecting the particles between the dividers. For example, some systems, such as centrifugal concentrators, may use rotating bowls having riffles or dividers disposed on inner surfaces of the bowls, 20 such that particle flow upward and out of the bowl on an inner surface of the bowl is impeded by the dividers and high density particles may be retained in retainers or recesses therebetween. However, some known systems for separating particles may have features and/or geometry that may not facilitate efficient separation of particles by density.

25

SUMMARY

In accordance with various embodiments, there is provided an apparatus for facilitating particle separation by density. The apparatus includes a separator having an inner surface surrounding a rotation axis of the separator and defining a 30 particle path from an input end of the separator to an axially spaced output end of

the separator, wherein the inner surface includes a plurality of axially spaced dividers having respective inner positions, the dividers defining at least in part respective axially spaced retainers for collecting particles during rotation of the separator, each of the retainers including at least one fluid inlet for fluidizing
5 particles in the retainer during operation. The plurality of dividers include a first pair of adjacent dividers and a second pair of adjacent dividers, the first pair of adjacent dividers nearer the input end than the second pair of adjacent dividers, wherein a first divider slope relative to the rotation axis between inner positions of the first pair of adjacent dividers is greater than a second divider slope relative to
10 the rotation axis between inner positions of the second pair of adjacent dividers and wherein each of the first and second divider slopes is zero or positive.

The first and second divider slopes may include first and second ratios of radial position difference over axial position difference respectively.

15

The first divider slope may be greater than about **10** degrees.

The first divider slope may be greater than about **20** degrees.

20

The second divider slope may be less than about **10** degrees.

The plurality of dividers may include a third pair of adjacent dividers, the third pair of adjacent dividers nearer the output end than the second pair of adjacent dividers, wherein a third divider slope relative to the rotation axis between inner
25 positions of the third pair of adjacent dividers is zero or positive and is less than the second divider slope.

The third divider slope may be less than about **10** degrees.

30

The third divider slope may be less than about **3** degrees.

5 The plurality of dividers may include a fourth pair of adjacent dividers, the fourth pair of adjacent dividers nearer the output end than the third pair of adjacent dividers, wherein a fourth divider slope relative to the rotation axis between inner positions of the fourth pair of adjacent dividers is zero or positive and is less than the third divider slope.

The fourth divider slope may be less than about **10** degrees.

10 The fourth divider slope may be less than about **3** degrees.

The plurality of dividers may include a fourth pair of adjacent dividers, the fourth pair of adjacent dividers nearer the output end than the third pair of adjacent dividers, wherein a fourth divider slope relative to the rotation axis between inner positions of the fourth pair of adjacent dividers is less than about **10** degrees.

15 The fourth divider slope may be less than about **3** degrees.

The inner positions for the dividers may lie on a parabolic path.

20 Respective divider slopes relative to the rotation axis between inner positions for each of the pairs of adjacent dividers may decrease from the input end to the output end of the separator.

25 A difference between two of the divider slopes may represent an angular difference of at least about **20** degrees.

30 The retainers may include a first pair of adjacent retainers and a second pair of adjacent retainers, the first pair of adjacent retainers nearer the input end than the second pair of adjacent retainers, wherein a first retainer slope relative to the rotation axis between retainer positions of the first pair of adjacent retainers is greater than a second retainer slope relative to the rotation axis between retainer

positions of the second pair of adjacent retainers, the first and second retainer slopes being zero or positive.

The second retainer slope may be less than about 3 degrees.

5

The retainers may include a third pair of adjacent retainers, the third pair of adjacent retainers nearer the output end than the second pair of adjacent retainers, wherein a third retainer slope relative to the rotation axis between retainer positions of the third pair of adjacent retainers is zero or positive and less than about 3
10 degrees.

The retainers may have common minimum depths.

15

In accordance with various embodiments, there is provided a system for facilitating particle separation by density. The system includes the apparatus as described above, a rotation driver coupled to the apparatus for causing the separator of the apparatus to rotate about the rotation axis, and a particle source in particle communication with the input end of the separator and configured to provide particles to the input end of the separator while the separator rotates about the
20 rotation axis.

Other aspects and features of embodiments of the present disclosure will become apparent to those ordinarily skilled in the art upon review of the following description of specific embodiments of the present disclosure in conjunction with the
25 accompanying figures.

BRIEF DESCRIPTION OF THE DRAWINGS

In drawings which illustrate embodiments of the present disclosure,

Figure 1 is a sectional side view of a system for facilitating particle separation by density according to various embodiments of the present disclosure;

5 Figure 2 is a sectional side view of a portion of the system shown in Figure 1 according to various embodiments of the present disclosure;

Figure 3 is a sectional side view of a separator of the system shown in Figure 1 according to various embodiments of the present disclosure;

10

Figure 4 is a sectional side view of a portion of a system for facilitating particle separation by density according to various embodiments of the present disclosure; and

15 Figure 5 is a sectional side view of a portion of a system for facilitating particle separation by density according to various embodiments of the present disclosure.

DETAILED DESCRIPTION

20 Referring to Figure 1, there is shown a sectional view of a system 10 for facilitating particle separation by density, in accordance with various embodiments. In various embodiments, the system 10 may act as a centrifugal concentrator.

25 Referring to Figure 1, the system 10 includes a separator 12 configured to rotate about a rotation axis 14. In some embodiments, the separator 12 may be referred to as a bowl. In various embodiments, the separator 12 may have properties and/or geometry that facilitates improved particle separation by density during operation. In various embodiments, the system 10 may include a motor 16 acting as a rotation driver coupled to the separator 12 for causing the separator to rotate
30 about the rotation axis 14 during use. For example, in some embodiments, the

motor **16** may be coupled to the separator **12** via a drive belt **18** and a drive shaft **19**.

The system **10** may include a particle source **20** in particle communication with an input end of the separator **12** and configured to provide particles while the separator rotates about the rotation axis **14**. For example, in various embodiments, the particle source **20** may include a feed tube. In some embodiments, the particles provided via the feed tube may be mixed in a slurry of water. For example, in some embodiments, a ratio of **60%** water and **40%** particles may be provided to the separator **12** by the particle source **20**. For example, in some embodiments, the particle source **20** may provide about **500** metric tonnes per hour of solids. In some embodiments, different embodiments generally similar to the system **10** may be configured to process particles provided at rates from **50** kg/hr to more than **500** metric tonnes per hour of solids, for example.

In various embodiments, the particles may include high density particles, such as, for example, gold particles along with other particles of lower density, such as rocks, sand, and/or soil. In some embodiments, the separator **12** may be configured to separate the high density particles from the lower density particles as the separator **12** rotates about the rotation axis **14**.

Referring to Figure **2**, an enlarged view of a portion (shown at **32** in Figure **1**) of the system **10** including the separator **12** is shown, which depicts further detail of the separator **12** in accordance with various embodiments. Referring to Figure **2**, the separator **12** includes an inner surface **100** surrounding the rotation axis **14** of the separator **12**. In various embodiments, the separator **12** may be made of a material or combination materials that is abrasion resistant and/or wear resistant, such as, for example, steel backing with a polyurethane cover/coating. In some embodiments, the separator **12** may include alternative or additional materials, such as, metal (e.g. steel), polyurethane, rubber, silicon carbide and/or combinations thereof. In various embodiments, the inner surface **100** may define

a particle path from an input end **102** of the separator **12** to an axially spaced output end **104** of the separator **12**.

Referring to Figure **2**, in various embodiments, the inner surface **100** may include
5 axially spaced dividers **120**, **122**, **124**, **126**, **128**, **130**, **132**, **134**, **136**, **138**, and **140**.
In various embodiments, each of the dividers **120-140** may have a respective inner
position relative to the rotation axis. In various embodiments, the inner position for
a divider may be defined as the position of the innermost surface of the divider
(e.g., an inner apex of the divider, closest to the rotation axis **14**). In some
10 embodiments, the dividers **120-140** may be generally annular, surrounding the
rotation axis **14**. In various embodiments, the dividers **120-140** may be generally
symmetrical about the rotation axis **14**.

In some embodiments, an inner position for each divider **120-140** may be
15 expressed as a two coordinate position for the innermost surface of the divider: a
radial position or measurement of distance from the rotation axis and an axial
position or measurement along the rotation axis. For example, referring to Figure
3, the separator **12** according to various embodiments, is shown in a cross
sectional view, in isolation. Referring to Figure **3**, a radial position measurement
20 for the divider **122** is shown at **252** and an axial position measurement depicting
the axial position of the divider **122** is shown at **254**. In the embodiment shown in
Figure **3**, the axial position measurement may be a relative position and may be
taken relative to a position of the divider **120**, which is nearest the input end **102**,
and so the divider **120** may be considered to be at an axial position of **0**. A radial
25 position measurement for the divider **120** is shown at **250**.

Referring to Figure **2**, in various embodiments, the dividers **120-140** may define
respective axially spaced retainers **152**, **154**, **156**, **158**, **160**, **162**, **164**, **166**, **168**,
and **170** for collecting particles during rotation of the separator **12**. In some
30 embodiments, the separator **12** may also include a retainer **150**. In some
embodiments, the retainers may be generally symmetrical about the rotation axis

14. In some embodiments, each of the retainers **150-170** may include a set of fluid inlets for fluidizing particles in the retainer during operation. For example, in some embodiments, fluid inlets for the retainer **152** shown in Figure **2** may include holes or passages along an outer radial wall of the retainer **152** (see for example, fluid inlet **180**). In some embodiments, the fluid inlets may be in fluid communication with a fluid reservoir **200** surrounding the separator **12**. For example, in some embodiments, the separator **12** may include about **400** holes or fluid inlets in each of the retainers with spacing of about **10** mm between the holes. In some embodiments, each of the retainers **150-170** of the separator **12** may include two axially spaced rows of fluid inlets, as shown in Figure **2**.

Referring still to Figure **2**, in various embodiments, the dividers **120-140** of the separator **12** may be positioned and/or configured to facilitate separation of particles by density that may be effective for both large and small particles. For example, in some embodiments, a difference in inner positions over axial displacement or slope for adjacent dividers may be lower for adjacent dividers near the output end **104** than it is for adjacent dividers near the input end **102**, as described in further detail below and this may, in some embodiments facilitate improved particle separation.

20

Referring to Figure **2**, in some embodiments, for a first pair of adjacent dividers **120** and **122** and a second pair of adjacent dividers **122** and **124**, the first pair nearer the input end **102** than the second pair, a first divider slope relative to the rotation axis between inner positions of the first pair of adjacent dividers **120** and **122** may be greater than a second divider slope relative to the rotation axis between inner positions of the second pair of adjacent dividers **122** and **124**. In various embodiments, the first and second divider slopes may be zero or positive (i.e., not negative), such that the divider **124** is not closer to the rotation axis than the divider **122** and the divider **122** is not closer to the rotation axis than the divider **120**.

30

In some embodiments, this reduction in divider slope may occur for respective pairs of adjacent dividers as they are considered from the input end **102** to the output end **104**, as described in further detail below.

- 5 In some embodiments, this change in slope may allow the dividers near the input end **102** to separate or capture coarser high density particles while the dividers near the output end **104** separate or capture finer high density particles. In various embodiments, keeping the slope of the second pair of adjacent dividers zero or positive (i.e., not negative) may facilitate continued movement of the particles
10 towards the output end, without excess build up of particles.

Operation

- Referring to Figure **1**, as discussed above, the system **10** may facilitate particle separation by density. In various embodiments, a mixture of particles and fluid,
15 such as for example, a **60-40** mixture of water and particles or slurry, may be provided by the particle source **20** to the input end **102** of the separator **12**. In some embodiments, the slurry including the particles may be gravity fed through the particle source **20** to the input end **102** of the separator **12**. In some embodiments,
20 the slurry may be first size separated using a vibrating screen, for example, before being provided to the separator **12**. In some embodiments, the particle source **20** may include a pump configured to pump the slurry into the input end **102** of the separator **12**.

- In various embodiments, while the particles are provided to the input end **102**, the
25 motor **16** may drive the separator **12** via the drive belt **18** and the drive shaft **19**. For example, in some embodiments, the separator **12** may be driven at a nominal rotational speed of about **400** rpm by the motor **16** drawing **75** kW of power and rotating at about **1485** rpm.

- 30 Referring to Figure **2**, the particles may be urged outward to the inner surface **100** of the separator **12** by the rotation of the separator **12** about the rotation axis **14**.

Referring to Figure 2, the inner surface **100** may include sloped walls **220** which may cause outward centrifugal forces to urge the particles upwards from the input end **102** towards the output end **104** of the separator **12**.

5 The particles may first enter the retainer **150** shown in Figure 2. In some embodiments, once the retainer is filled with particles, some particles may pass over the divider **120** into the adjacent retainer **152** shown in Figure 2. In various
10 embodiments, the particles that remain in the retainer **150** may include particles having higher density than those which pass over the divider **120** into the adjacent
retainer **152**. In various embodiments, the separator **12** may include fluid inlets, such as the fluid inlet **180**, for example, in fluid communication with each of the
retainers **150-170** to facilitate settling of higher density particles within the retainers. In various embodiments, the fluid inlets may include holes or passages
15 in fluid communication with the reservoir **200** and the inner surface **100**. In operation, water may be kept under pressure in the fluid reservoir **200** and the
pressure of the water may cause the water to flow through the fluid inlets into the retainers **150-170**.

Referring to Figure 2, in various embodiments, the retainer **152** may be defined at
20 least in part by the dividers **120** and **122**. In various embodiments, once the retainer **152** is filled with particles, the particles may pass over the divider **122** into
the retainer **154**.

In various embodiments, an ease or rate at which the particles pass over the
25 divider **122** may depend at least in part on a divider slope relative to the rotation axis **14** between inner positions of the dividers **120** and **122**. In some
embodiments, the divider slope may be determined as a ratio of radial position
difference over axial position difference for the inner positions of the dividers **120**
and **122**. In various embodiments, the radial position of the divider **120** may be the
30 radial distance or measurement between the innermost surface of the divider **120**
and the rotation axis **14**. For example, in some embodiments, the innermost

surface of the divider **120** may be about **440** mm from the rotation axis **14** and so the radial position of the divider **120** may be about **440** mm. The radial position of the divider **122** may be determined similarly to be about **466** mm.

5 Referring to Figure **3**, the separator **12** according to various embodiments, is shown in isolation. Referring to Figure **3**, the measurement depicting the radial position of the divider **120** is shown at **250** and the measurement depicting the radial position of the divider **122** is shown at **252**.

10 In various embodiments, the axial position of the divider **120** may be a position projected on the rotation axis **14** of the innermost surface of the divider **120**. In some embodiments, where the innermost surface of the divider **120** may extend axially such that a cylindrical surface is provided, for example, an axial position of the divider may be the average axial position of the innermost surface of the
 15 divider. In some embodiments, axial positions may be measured relative to the divider closest to the input end **102** and so the divider **120** may be considered to have an axial position of **0** mm. In some embodiments, the divider **122** may have an axial position of about **48** mm. Referring to Figure **3**, the measurement showing the axial position of the divider **122** is shown at **254**. In some embodiments, the
 20 dividers **120-138** may each have an axial surface height of about **6.4** mm, for example.

In various embodiments, the divider slope may be determined by the following equation:

25

$$m_{div} = \frac{r_{div2} - r_{div1}}{p_{div2} - p_{div1}}$$

where r_{div1} is the radial position of the divider **120**, r_{div2} is the radial position of the divider **122**, p_{div1} is the axial position of the divider **120**, and p_{div2} is the axial
 30 position of the divider **122**.

Accordingly, in various embodiments, the divider slope for the pair of adjacent dividers **120** and **122** may be about $(466-440)/(48-0)=0.542$. In some embodiments, the divider slope may be expressed in degrees (i.e., about $\tan^{-1}(26/48) = 28.4$ degrees). In various embodiments, the divider slope for the pair of adjacent dividers **120** and **122** may be positive, such that the divider **122** near the output end has a larger radial position than the divider **120**, to facilitate flow of particles from the input end **102** to the output end of the separator **12** when the separator **12** rotates about the rotation axis **14**.

In various embodiments, some particles that pass over the divider **122** may next pass over the divider **124** and enter the retainer **154** shown in Figure 2. In various embodiments, the particles that do not pass over the divider **124** and remain in the retainer **152** may include particles having higher density than those which pass over the divider **124** into the adjacent retainer **154**.

In various embodiments, the divider slope for the pair of adjacent dividers **122** and **124** may be less than the divider slope for the pair of adjacent dividers **120** and **122**. In various embodiments, the divider slope for the pair of adjacent dividers **122** and **124** may be zero or positive (i.e., not negative). In various embodiments, this may facilitate flow of particles from the input end **102** to the output end of the separator **12**. For example, in some embodiments, the divider **124** may have a radial position of about **489** mm and an axial position of about **97** mm. Accordingly, the divider slope for the pair of adjacent dividers **122** and **124** may be about $(489-466)/(97-48) = 0.469$ or **25.1** degrees.

In various embodiments, having the divider slope for the pair of adjacent dividers **120** and **122** greater than the divider slope for the pair of adjacent dividers **122** and **124**, which are downstream from the dividers **120** and **122**, while keeping the divider slope zero or positive, may facilitate improved separation of particles by density. For example, in some embodiments, where high density particles such

as gold are to be recovered using the system **10**, higher recovery rates may be facilitated. In some embodiments, the improved separation may result from the dividers **120** and **122** shown in Figure **1** being better suited for capturing larger high density particles in the retainer **152** whereas the dividers **122** and **124** may be better suited for capturing smaller high density particles in the retainer **154**. In various embodiments, by keeping the divider slope zero or positive (i.e., non-negative), the particles may be encouraged to flow and improved particle separation may be facilitated.

In various embodiments, particles may next pass over the divider **126** and enter the retainer **156** shown in Figure **2**. In various embodiments, the particles that remain in the retainer **154** may include particles having higher density than those which pass over the divider **126** into the adjacent retainer **156**. In various embodiments, the divider slope for the pair of adjacent dividers **124** and **126** may be less than the divider slope for the pair of adjacent dividers **122** and **124**, but still not negative). For example, in some embodiments, the divider **126** may have a radial position of about **511** mm and an axial position of about **145** mm. Accordingly, the divider slope for the pair of adjacent dividers **124** and **126** may be about **0.458** or about **24.6** degrees.

In various embodiments, having the divider slope for the pair of adjacent dividers **122** and **124** greater than the divider slope for the pair of adjacent dividers **124** and **126** while also having the divider slope for the pair of adjacent dividers **120** and **122** greater than the divider slope for the pair of adjacent dividers **122** and **124** may facilitate improved separation of particles by density. For example, in some embodiments, where high density particles such as gold are to be recovered using the system **10**, higher recovery rates may be facilitated.

In some embodiments, the improved separation may result from the dividers **120** and **122** shown in Figure **2** being better suited for capturing larger high density particles in the retainer **152** whereas the dividers **122** and **124** and then **124** and

126 may be better suited for capturing progressively smaller high density particles in the retainers **154** and **156** respectively. In various embodiments, this progressive or stepped approach to particle separations may result in higher yields and/or more accurate particle separation by density. In various embodiments, by
5 keeping the divider slopes zero or positive (i.e., non-negative), the particles may be encouraged to flow and improved particle separation may be facilitated.

In various embodiments, particles may next pass over the divider **128** and enter the retainer **158** shown in Figure 2. In various embodiments, the particles that
10 remain in the retainer **156** may include particles having higher density than those which pass over the divider **128** into the adjacent retainer **158**. In various embodiments, the divider slope for the pair of adjacent dividers **126** and **128** may be less than the divider slope for the pair of adjacent dividers **124** and **126**. For example, in some embodiments, the divider **128** may have a radial position of
15 about **530** mm and an axial position of about **193** mm. Accordingly, the divider slope for the pair of adjacent dividers **126** and **128** may be about **0.396** or about **21.6** degrees.

In various embodiments, having a further divider slope where the slope is less and
20 zero or positive may facilitate further improved separation of particles by density. For example, in some embodiments, where high density particles such as gold are to be recovered using the system **10**, higher recovery rates may be facilitated. In some embodiments, the improved separation may result from the dividers **120** and
25 **122**, **122** and **124**, **124** and **126**, and **126** and **128** shown in Figure 2 being better suited for capturing progressively smaller high density particles in the retainers **152**, **154**, **156**, and **158** respectively. In various embodiments, by keeping the divider slope zero or positive, the particles may be encouraged to flow and improved particle separation may be facilitated.

30 In various embodiments, each additional pair of dividers with a reduced divider slope may facilitate improved separation of particles by density.

Referring to Figure 2, during operation, rotation of the separator **12** about the rotation axis **14** may cause the particles to continue to flow from the input end **102** to the output end **104**, over the dividers **120-140**. Referring now to Figure 1, some particles will flow upwards over the divider **140** (shown in Figure 2) and then outwards over the top of the separator **12**. In various embodiments, these particles may flow out of the system **10** via a sloped output slide **30**.

Referring to Figure 2, the dividers **130**, **132**, **134**, **136**, and **138** may have radial positions and axial positions of (**548** mm, **241** mm), (**563** mm, **290** mm), (**576** mm, **338** mm), (**584** mm, **389** mm), and (**584** mm, **437** mm) respectively. Accordingly, in various embodiments, the divider slopes for the pairs of adjacent dividers **120** and **122**, **122** and **124**, **124** and **126**, **126** and **128**, **128** and **130**, **130** and **132**, **132** and **134**, **134** and **136**, and **136** and **138** may be about **0.542** or about **28.4** degrees, about **0.469** or about **25.1** degrees, about **0.458** or about **24.6** degrees, about **0.396** or about **21.6** degrees, about **0.375** or about **20.6** degrees, about **0.306** or about **17.0** degrees, about **0.271** or about **15.15** degrees, about **0.157** or about **8.9** degrees, and about **0** or about **0** degrees, respectively.

In various embodiments, a difference between divider slopes for at least two of the divider slopes may represent an angular difference of at least about **20** degrees. For example, in various embodiments, the difference between the divider slopes for the pair of adjacent dividers **120** and **122** and the pair of adjacent dividers **136** and **138** may represent an angular difference of about **28.4** degrees. In some embodiments, this minimum difference in slopes may facilitate accurate separation by density of differing particle sizes.

In various embodiments, the divider slopes for pairs of adjacent dividers may decrease for each pair from the input end **102** to the output end **104**. For example, in some embodiments, the divider slopes for pairs of adjacent dividers may decrease for the pairs of adjacent dividers **120** and **122**, **122** and **124**, **124** and

126, 126 and 128, 128 and 130, 130 and 132, 132 and 134, 134 and 136, and 136 and 138 as they progress from the input end **102** to the output end **104**. In some embodiments, this progressive reduction of divider slopes while the slopes remain zero or positive (i.e., non-negative) may facilitate particle separation by density of progressively finer particles in the retainers **152-168**.

In some embodiments, including the pair of adjacent dividers **136** and **138** which have a small divider slope near the output end after progressively decreasing divider slopes may facilitate particle separation of high density fine particles by the separator **12**. For example, in some embodiments, the pair of adjacent dividers **136** and **138** may have a divider slope of less than about **10** degrees and this may facilitate particle separation of high density fine particles by the separator. In some embodiments, the pair of adjacent dividers **136** and **138** may have a divider slope of about zero degrees and this may facilitate particle separation of high density fine particles. In some embodiments, a slope of about zero degrees may be a slope of less than about **3** degrees.

Referring to Figure **2**, in some embodiments, the separator **12** may include a divider **140** near the output end. In some embodiments, the divider **140** may be adjacent to the divider **138** and may have a radial position and axial position of (**584** mm and **492** mm), such that the pair of adjacent dividers **138** and **140** have a divider slope of about **0**. In some embodiments, including the retainers **168** and **170** defined by respective pairs of dividers which both have a small divider slope near the output end after progressively decreasing divider slopes may facilitate particle separation of high density fine particles by the separator **12**. For example, in some embodiments, the pairs of adjacent dividers **136** and **138** and **138** and **140** may each have a divider slope of less than about **10** degrees and this may facilitate particle separation of high density fine particles by the separator. In some embodiments, the pairs of adjacent dividers **136** and **138** and **138** and **140** may each have a divider slope of about zero degrees and this may facilitate particle separation of high density fine particles.

In some embodiments, centrifugal force generated by rotation of the separator **12** may push the particle slurry against the inner surface **100** shown in Figure **2** and create an interface between the particle slurry and the atmosphere inside the separator **12**. In some embodiments, the angle of this interface may be between about **5** degrees and about **10** degrees from the vertical axis of rotation. The angle may depend at least in part on the size of the particles within the slurry and the solids density of the slurry. Coarser particles (e.g., **2.0mm**) and higher solids density (e.g., **60%** solids) may result in a higher angle (e.g. about **10** degrees in some embodiments). Finer particles (e.g., **0.1mm**) and lower solids density (e.g., **20%** solids) may result in a lower angle (e.g. **5** degrees).

In some embodiments, the separator **12** may facilitate effective recovery of both coarse and fine heavy mineral particles by changing divider slopes from the input end **102** to the output end **104** such that some divider slopes are greater than the angle of the interface or axially inside of the slurry face and some divider slopes are less than the angle of the interface or axially outside of the slurry face. In some embodiments, pairs of adjacent dividers having divider slopes greater than the angle of the interface may effectively recover relatively coarser heavy mineral particles and pairs of adjacent dividers having divider slopes less than the angle of the interface may effectively recover relatively finer heavy mineral particles.

Accordingly, in some embodiments, at least one pair of adjacent dividers may have a divider slope of greater than the angle of the interface, such as, for example, greater than about **10** degrees. In some embodiments, at least one pair of adjacent dividers may have a divider slope of much greater than **10** degrees, such as, for example greater than **20** degrees, to facilitate particle separation of coarser particles. For example, in some embodiments, the divider slope for the pair of adjacent dividers **120** and **122** may be greater than about **20** degrees. In some embodiments, at least one pair of adjacent dividers nearer the output end **104** of the separator **12** may have a divider slope of less than the angle of the interface,

such as, for example, less than about **10** degrees. For example, in some embodiments, the divider slope for each of the pairs of adjacent dividers **134** and **136**, **136** and **138**, and **138** and **140** may be less than about **10** degrees. In some embodiments, a progression of divider slopes from greater than **20** degrees to less than **10** degrees may promote slurry flow from the input end **102** to the output end **104** of the separator **12**.

In some embodiments, the inner positions of at least some of the dividers **120-140** may lie generally on a parabolic path. For example, in some embodiments, inner positions for at least four of the dividers may generally lie on a parabolic path. Referring to Figure **2**, in some embodiments, the inner position of each of the dividers **120-134** may be determined generally using a parabolic function. For example, in some embodiments, the inner positions may follow the following parabolic function:

$$r = -4.460851806 \cdot 10^{-4} x^2 + 5.533849361 \cdot 10^{-1} x + 440.0538903$$

where r is the inner position in mm and x is the axial position in mm for each of the dividers **120-136**. In some embodiments, the above equation may be true within less than about **0.5%** of the radial position, for example, or in some embodiments, less than about **1** mm, for example, such that the inner positions for the dividers generally lie on a parabolic path. In some embodiments, using a generally parabolic path may facilitate improved particle separation by density. For example, in some embodiments, particle/material flow may be facilitated by following a smooth path as provided by a parabolic path, for example, and this may result in improved particle separation when compared to a path having abrupt changes in flow direction, for example.

Referring to Figure **2**, in some embodiments, the configuration of the retainers **150-170** may facilitate improved particle separation by density. For example, in some embodiments, the retainers **150-170** may slope outwards more near the input end

102 than near the output end **104** of the separator **12**. In various embodiments, this may allow the retainers **150-170** to keep a consistent depth and may facilitate separation of larger particles near the input end **102** and separation of smaller particles near the output end **104**. In some embodiments, the retainers **150-170**
5 may have common depths. For example, in some embodiments the retainers **150-170** may have common minimum depths, measured radially, of about **25** mm.

In some embodiments, lower retainer volumes may improve concentrate grade (e.g., amount of target material vs. total amount of material collected) as the target
10 material may be only collected on the surface of the retainers. However, in some embodiments, a minimum depth may be required so the water from the fluid inlets does not blow the target material (e.g. gold) off the surface of the retainers. Accordingly, in various embodiments, common minimum depths may be employed. In various embodiments, use of a depth of about **25** mm in the
15 separator **12** shown in Figure **2** to facilitate separation may be determined to be effective empirically.

Referring to Figure **2**, in some embodiments, each of the retainers **150-170** may have a respective retainer position relative to the rotation axis. In some
20 embodiments, the retainer position for a retainer may be defined as the position of the central surface of the retainer (e.g., the position of the surface of the retainer midway between adjacent dividers defining the retainer). In some embodiments, the retainer position for a retainer may be defined as the position or average position of the outermost particle engaging surface of the retainer. In some
25 embodiments, each of the retainer positions may be expressed using coordinates and may include a radial position and a relative axial position. For example, referring to Figure **3**, the retainer **152** may have a retainer position including a radial position shown at **290** and an axial position of **0**. Referring still to Figure **3**, the retainer **154** may have a retainer position including a radial position shown at
30 **292** and an axial position shown at **294**, measured from the axial position of the retainer **152**.

In some embodiments, the retainers **150-170** may include a first pair of adjacent retainers **152** and **154** and a second pair of adjacent retainers **154** and **156**, the first pair of adjacent retainers nearer the input end **102** than the second pair of adjacent retainers, wherein a first retainer slope relative to the rotation axis between retainer positions of the first pair of adjacent retainers is greater than a second retainer slope relative to the rotation axis between retainer positions of the second pair of adjacent retainers and wherein the first and second retainer slopes are zero or positive. In some embodiments, this slope relationship may result in the retainers **152** and **154** sloping outwards more than the retainers **154** and **156**. In various embodiments, this may allow the retainers to keep a consistent depth and may facilitate separation of larger particles near the input end **102** and separation of smaller particles near the output end **104**.

In some embodiments, the retainer slope for the pair of adjacent retainers **152** and **154** may be determined using the following equation:

$$m_{ret} = \frac{r_{ret2} - r_{ret1}}{p_{ret2} - p_{ret1}}$$

where r_{ret1} is the radial position of the retainer **152**, r_{ret2} is the radial position of the retainer **154**, p_{ret1} is the axial position of the retainer **152**, and p_{ret2} is the axial position of the retainer **154**.

For example, in some embodiments, the retainer **152** may have a radial position of **290** and an axial position of **0** mm. In some embodiments, the retainer **154** may have a radial position of **515** mm and an axial position of **48** mm. In some embodiments, the retainer **154** may have a radial position of **515** and an axial position of **96** mm. Accordingly the retainer slope for the pair of adjacent retainers **152** and **154** may be calculated as about **0.500** or about **26.6** degrees. In some embodiments, the retainer **156** may have a radial position of **536** and an axial

position of **144** mm. Accordingly the retainer slope for the pair of adjacent retainers **154** and **156** may be calculated as about **0.438** or about **23.6** degrees. Accordingly, in various, embodiments, the retainer slope for the pair of adjacent retainers **152** and **154** may be greater than the retainer slope for the pair of adjacent retainers **154** and **156**.

In various embodiments, the retainers **158**, **160**, **162**, **164**, **166**, **168**, and **170** may have retainer positions (radial position, axial position) of about (**536** mm, **96** mm), (**556** mm, **145** mm), (**573** mm, **193** mm), (**589** mm, **241** mm), (**602** mm, **289** mm), (**610** mm, **340** mm), (**610** mm, **389** mm), and (**610** mm, **437** mm) respectively. Accordingly, the retainer slopes for pairs of adjacent retainers **156** and **158**, **158** and **160**, **160** and **162**, **162** and **164**, **164** and **166**, **166** and **168**, and **168** and **170** may be about **0.408**, **0.354**, **0.333**, **0.271**, **0.157**, **0**, and **0** respectively.

Accordingly, in various embodiments, the retainer slopes may progressively diminish from the input end **102** to the output end **104**. In various embodiments, each pair of adjacent retainers that has a progressively diminishing retainer slope may facilitate improved particle separation.

In some embodiments, the retainer **150** may have a radial position of **465** mm and an axial position of **-48** mm. Accordingly, the retainer slope for the pair of adjacent retainers **150** and **152** may be calculated as **0.542** or **28.4** degrees.

In some embodiments, the retainer slope between adjacent retainers **166** and **168** may be small. For example in some embodiments, the retainer slope between the adjacent retainers **166** and **168** may be less than about **10** degrees. In some embodiments, the retainer slope may be about zero or less than about **3** degrees. In some embodiments, having a small retainer slope of for at least one pair of adjacent retainers near the output end **104** may facilitate separating small particles near the output end. In some embodiments, the slope between adjacent retainers **168** and **170** may also be small, such that there are two pairs of adjacent retainers

that have a retainer slope of about zero near the output end **104**. In some embodiments, having more than one pair of adjacent retainers with a small slope near the output end **104** may facilitate more efficient separation of small particles by the system **10**.

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Referring to Figure **1**, in some embodiments, after the system **10** has been run for a separation time period, during which the separator **12** has rotated about the rotation axis **14** and particles have built up within the retainers **150-170** (shown in Figure **2**), the separator **12** may cease rotating and the particles may be recovered from the retainers **150-170**. In various embodiments, particles that remain in the retainers **150-170** may include particles having higher density than those which flow upwards out of the output end **104** of the separator **12**. In some embodiments, the separation time period may be about **30** to **60** minutes, for example. In various embodiments, the system **10** may be repeatedly run, with new particles input into the separator **12** and the separator **12** rotated about the rotation axis **14** for each run.

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Separator embodiments

In various embodiments, other separators or bowls that facilitate functionality generally similar to the separator **12** shown in Figures **1-3** may be used to facilitate particle separation by density generally as described herein regarding the separator **12**.

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Referring to Figure **4**, there is shown a portion of a system according to various embodiments, which may include functional features generally similar to the system **10** shown in Figure **1** and discussed above. Referring to Figure **4**, the system may include a separator **302**, which may function generally similarly to the separator **12** described above and shown in Figures **1-3**. In various embodiments, the separator **302** may be smaller than the separator **12**, and may be configured to facilitate particle separation by density with lower throughput than the separator **12**.

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In operation, the system may include a motor acting as a rotation driver coupled to the separator **302** for causing the separator to rotate about a rotation axis **304** during use. In some embodiments, the system may include a particle source in particle communication with an input end **308** of the separator **302** and configured to provide particles while the separator rotates about the rotation axis **304**. In various embodiments, while the particles are provided at the input end **308**, the motor may drive rotation of the separator **302** about the rotation axis **304**.

Referring to Figure 4, the particles may be urged outward to an inner surface **306** of the separator **302** by the rotation of the separator **302** about the rotation axis **304**. Referring to Figure 4, the inner surface **306** may be generally sloped outward which may cause outward centrifugal forces to urge the particles upwards from the input end **308** towards an output end **310** of the separator **302**.

Referring to Figure 4, the inner surface **306** of the separator **302** may surround the rotation axis **304** and define a particle path from the input end **308** to the axially spaced output end **310**. In various embodiments, the inner surface **306** may include axially spaced dividers **320**, **322**, **324**, **326**, **328**, and **330** having respective inner positions, the dividers defining at least in part respective axially spaced retainers **340**, **342**, **344**, **346**, and **348** for collecting particles during rotation of the separator. In various embodiments, each of the retainers **340-348** may include fluid inlets for fluidizing particles in the retainer during operation. For example, the retainer **340** may include holes or fluid passages (e.g., including those shown at **360** and **362**), which are in fluid communication with a fluid reservoir **370**. In operation, water may be kept under pressure in the fluid reservoir **370** and the pressure of the water may cause the water to flow through the fluid inlets into the retainers **340-348**.

In some embodiments, the dividers **320-330** may include a first pair of adjacent dividers **320** and **322** and a second pair of adjacent dividers **322** and **324**, the first pair of adjacent dividers nearer the input end **308** than the second pair of adjacent dividers. In various embodiments, a first divider slope relative to the rotation axis

between inner positions of the first pair of adjacent dividers **320** and **322** may be greater than a second divider slope relative to the rotation axis between inner positions of the second pair of adjacent dividers **322** and **324**. Each of the first and second divider slopes may be non-negative slopes, which may in some
5 embodiments encourage flow of particles from the input end **308** to the output end **310**.

In various embodiments, the difference in slopes between the first pair of adjacent dividers and the second pair of adjacent dividers may facilitate improved separation
10 of particles by density for at least the reasons provided above having regard to the separator **12** shown in Figures **1-3**.

Referring to Figure **4**, in various embodiments, the dividers **320**, **322**, **324**, **326**, **328**, and **330** may have inner positions (radial position, axial position) of about (**131** mm,
15 **0** mm), (**143** mm, **30** mm), (**155** mm, **66**mm), (**164** mm, **99** mm), (**170** mm, **134** mm), and (**175** mm, **174.5** mm). Accordingly, in various embodiments the slopes between adjacent pairs of dividers **320** and **322**, **322** and **324**, **324** and **326**, **326** and **328**, and **328** and **330** may be about **0.400**, **0.333**, **0.273**, **0.171**, and **0.123** respectively. In various embodiments, each pair of adjacent dividers that has a progressively
20 diminishing divider slope may facilitate improved particle separation, for example, as described above having regard to the separator **12** shown in Figures **1-3**.

In some embodiments, the inner positions for the dividers **320**, **322**, **324**, **326**, **328**, and **330** may lie on a parabolic path, such as for example, the parabolic path defined
25 by the following function:

$$r = -1.040500288 \cdot 10^{-3} x^2 + 4.331438342 \cdot 10^{-1} x + 130.9909349$$

where r is the inner position in mm and x is the axial position in mm for each of the
30 dividers **320-330**.

Referring still to Figure 4, in various embodiments, the configuration of the retainers **340-348** may facilitate improved particle separation by density. For example, in some embodiments, the retainers **340-348** may slope outwards more for adjacent retainers near the input end **308** than for adjacent retainers near the output end **310** of the separator **302**. In various embodiments, the retainers **340-348** may have retainer positions (radial position, axial position) of about (**158 mm, 0 mm**), (**170 mm, 34 mm**), (**181 mm, 68 mm**), (**189 mm, 102 mm**), and (**195 mm, 136 mm**) respectively. Accordingly, in various embodiments the retainer slopes for pairs of adjacent retainers **340** and **342**, **342** and **344**, **344** and **346**, and **346** and **348** may be about **0.353, 0.324, 0.235, and 0.176** respectively. In various embodiments, each pair of adjacent retainers that has a progressively diminishing retainer slope may facilitate improved particle separation.

Referring now to Figure 5, there is shown a portion of a system according to various embodiments, which may include functional features generally similar to the system **10** shown in Figure 1 and discussed herein. Referring to Figure 5, the system may include a separator **452**, which may function generally similarly to the separators **12** and **302** described above and shown in Figures 1-3 and 4.

In some embodiments, the system may include a motor acting as a rotation driver coupled to the separator **452** for causing the separator to rotate about a rotation axis **454** during use. In some embodiments, the system may include a particle source in particle communication with an input end **458** of the separator **452** and configured to provide particles while the separator rotates about the rotation axis **454**. In various embodiments, while the particles are provided at the input end **458**, the motor may drive rotation of the separator **452** about the rotation axis **454**.

Referring to Figure 5, the particles may be urged outward to an inner surface **456** of the separator **452** by the rotation of the separator **452** about the rotation axis **454**. Referring to Figure 5, the inner surface **456** may be generally sloped outward

which may cause outward centrifugal forces to urge the particles upwards from the input end **458** towards an output end **460** of the separator **452**.

Referring to Figure **5**, the inner surface **456** of the separator **452** may surround the rotation axis **454** and define a particle path from the input end **458** to the axially spaced output end **460**. In various embodiments, the inner surface **456** may include axially spaced dividers **470**, **472**, **474**, **476**, **478**, and **480** having respective inner positions, the dividers defining at least in part respective axially spaced retainers **490**, **492**, **494**, **496**, and **498** for collecting particles during rotation of the separator. In various embodiments, each of the retainers **490-498** may include fluid inlets for fluidizing particles in the retainer during operation. For example, the retainer **340** may include holes or fluid passages (e.g., including those shown at **510** and **512**), which are in fluid communication with a fluid reservoir **520**.

In some embodiments, the dividers **470-480** may include a first pair of adjacent dividers **470** and **472** and a second pair of adjacent dividers **472** and **474**, the first pair of adjacent dividers nearer the input end **458** than the second pair of adjacent dividers. In various embodiments, a first divider slope relative to the rotation axis between inner positions of the first pair of adjacent dividers **470** and **472** may be greater than a second divider slope relative to the rotation axis between inner positions of the second pair of adjacent dividers **472** and **474**. Each of the first and second divider slopes may be non-negative slopes, which may in some embodiments encourage flow of particles from the input end **458** to the output end **460**.

In various embodiments, the difference in slopes between the first pair of adjacent dividers and the second pair of adjacent dividers may facilitate improved separation of particles by density for at least the reasons provided above having regard to the separator **12** shown in Figures **1-3**.

Referring to Figure 5, in various embodiments, the divider **470** may have an inner position (corresponding to the innermost point of the divider **470**) of about (**129 mm, 0 mm**). In various embodiments, the dividers **470, 472, 474, 476, 478**, and **480** may have inner positions (radial position, relative axial position) of about (**129 mm, 0 mm**), (**153 mm, 48 mm**), (**162 mm, 80 mm**), (**168 mm, 112 mm**), (**171 mm, 142 mm**), and (**171 mm, 178 mm**). Accordingly, in various embodiments the slopes between adjacent pairs of dividers **470** and **472**, **472** and **474**, **474** and **476**, **476** and **478**, and **478** and **480** may be about **0.500, 0.281, 0.188, 0.100**, and **0** respectively.

10 In various embodiments, each pair of adjacent dividers that has a progressively diminishing divider slope may facilitate improved particle separation, for example, as described above having regard to the separator **12** shown in Figures **1-3**.

15 As discussed above, in some embodiments, having a small divider slope, which may be about zero, for example, near the output end **460** after having the divider slopes progressively decrease may facilitate capture and/or separation of fine particles near the output end **460**.

20 Referring still to Figure 5, in various embodiments, the configuration of the retainers **490-498** may facilitate improved particle separation by density. For example, in some embodiments, the retainers **490-498** may slope outwards more for adjacent retainers near the input end **458** than for adjacent retainers near the output end **460** of the separator **452**. In various embodiments, the retainers **490-498** may have retainer positions (radial position, relative axial position) of about (**167 mm, 0 mm**), (**182 mm, 32 mm**), (**187 mm, 63 mm**), (**187 mm, 94 mm**), and (**187 mm, 123 mm**) respectively. Accordingly, in various embodiments the slopes for pairs of adjacent retainers **490** and **492**, **492** and **494**, **494** and **496**, and **496** and **498** may be about **0.469, 0.161, 0**, and **0** respectively. In various embodiments, each pair of adjacent retainers that has a progressively diminishing retainer slope may facilitate improved particle separation.

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In some embodiments, the retainer slope for at least one pair of adjacent retainers may be small. For example, in some embodiments, the retainer slope may be less than about **10** degrees. In some embodiments, the retainer slope may be about **0** or less than about **3** degrees. For example, in some embodiments, there may be a
5 retainer slope of about **0** for the retainers **494** and **496** and **496** and **498**. In some embodiments, the retainer slope may be about zero for at least one retainer near the output end **460**. In some embodiments, this may help to facilitate improved particle separation of fine particles in the retainers **494**, **496** and **498** near the output end **460**.

10 Various embodiments

In some embodiments, some divider slopes may be negative, for example, near the output end **104** of the separator **12**.

In some embodiments, the separators **12**, **302** and/or **452** shown in Figures **2**, **4**, and
15 **5** may include distinct parts or portions coupled together. For example, in some embodiments, the inner surfaces **100**, **306**, and/or **456** may be made of two or more distinct parts that may be coupled together to form a generally continuous surface.

In some embodiments, two pairs of adjacent dividers, for which the divider slopes
20 may be compared, may include a common divider. In some embodiments, two pairs of adjacent dividers, for which the divider slopes may be compared may include only distinct dividers.

In some embodiments, two pairs of adjacent retainers, for which the retainer slopes
25 may be compared, may include a common retainer. In some embodiments, two pairs of adjacent retainers, for which the retainer slopes may be compared may include only distinct retainers.

While specific embodiments of the present disclosure have been described and
30 illustrated, such embodiments should be considered illustrative of the present

disclosure only and not as limiting the present disclosure as construed in accordance with the accompanying claims.

CLAIMS:

1. An apparatus for facilitating particle separation by density, the apparatus comprising:

5 a separator having an inner surface surrounding a rotation axis of the separator and defining a particle path from an input end of the separator to an axially spaced output end of the separator, wherein the inner surface includes a plurality of axially spaced dividers having respective inner positions, the dividers defining at least in part
10 respective axially spaced retainers for collecting particles during rotation of the separator, each of the retainers including at least one fluid inlet for fluidizing particles in the retainer during operation;

wherein the plurality of dividers include a first pair of adjacent dividers and a second pair of adjacent dividers, the first pair of adjacent
15 dividers nearer the input end than the second pair of adjacent dividers, wherein a first divider slope relative to the rotation axis between inner positions of the first pair of adjacent dividers is greater than a second divider slope relative to the rotation axis between inner positions of the second pair of adjacent dividers and wherein each of the first and second divider slopes is zero or positive.

- 20 2. The apparatus of claim 1 wherein the first and second divider slopes comprise first and second ratios of radial position difference over axial position difference respectively.
3. The apparatus of claim 1 or 2 wherein the first divider slope is greater than about 10 degrees.
- 25 4. The apparatus of claim 3 wherein the first divider slope is greater than about 20 degrees.

5. The apparatus of any one of claims **1** to **4** wherein the second divider slope is less than about **10** degrees.
- 5 6. The apparatus of any one of claims **1** to **5** wherein the plurality of dividers include a third pair of adjacent dividers, the third pair of adjacent dividers nearer the output end than the second pair of adjacent dividers, wherein a third divider slope relative to the rotation axis between inner positions of the third pair of adjacent dividers is zero or positive and is less than the second divider slope.
- 10 7. The apparatus of claim **6** wherein the third divider slope is less than about **10** degrees.
8. The apparatus of claim **7** wherein the third divider slope is less than about **3** degrees.
- 15 9. The apparatus of any one of claims **6** to **8** wherein the plurality of dividers include a fourth pair of adjacent dividers, the fourth pair of adjacent dividers nearer the output end than the third pair of adjacent dividers, wherein a fourth divider slope relative to the rotation axis between inner positions of the fourth pair of adjacent dividers is zero or positive and is less than the third divider slope.
- 20 10. The apparatus of claim **9** wherein the fourth divider slope is less than about **10** degrees.
11. The apparatus of claim **10** wherein the fourth divider slope is less than about **3** degrees.
- 25 12. The apparatus of claim **7** or **8** wherein the plurality of dividers include a fourth pair of adjacent dividers, the fourth pair of adjacent dividers nearer the output end than the third pair of adjacent dividers, wherein a fourth

divider slope relative to the rotation axis between inner positions of the fourth pair of adjacent dividers is less than about **10** degrees.

13. The apparatus of claim **12** wherein the fourth divider slope is less than about **3** degrees.

5 **14.** The apparatus of any one of claims **6** to **13** wherein the inner positions for the dividers lie on a parabolic path.

10 **15.** The apparatus of any one of claims **6** to **14** wherein respective divider slopes relative to the rotation axis between inner positions for each of the pairs of adjacent dividers decrease from the input end to the output end of the separator.

16. The apparatus of any one of claims **1** or **15** wherein a difference between two of the divider slopes represents an angular difference of at least about **20** degrees.

15 **17.** The apparatus of any one of claims **1** to **16** wherein the retainers include a first pair of adjacent retainers and a second pair of adjacent retainers, the first pair of adjacent retainers nearer the input end than the second pair of adjacent retainers, wherein a first retainer slope relative to the rotation axis between retainer positions of the first pair of adjacent retainers is greater than a second retainer slope relative to the rotation axis between retainer positions of the second pair of adjacent retainers, the first and second retainer slopes being zero or positive.

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18. The apparatus of claim **17** wherein the second retainer slope is less than about **3** degrees.

25 **19.** The apparatus of claim **17** or **18** wherein the retainers include a third pair of adjacent retainers, the third pair of adjacent retainers nearer the output end than the second pair of adjacent retainers, wherein a third retainer slope

relative to the rotation axis between retainer positions of the third pair of adjacent retainers is zero or positive and less than about **3** degrees.

20. The apparatus of any one of claims **1** to **19** wherein the retainers have common minimum depths.

5 **21.** A system for facilitating particle separation by density, the system comprising:

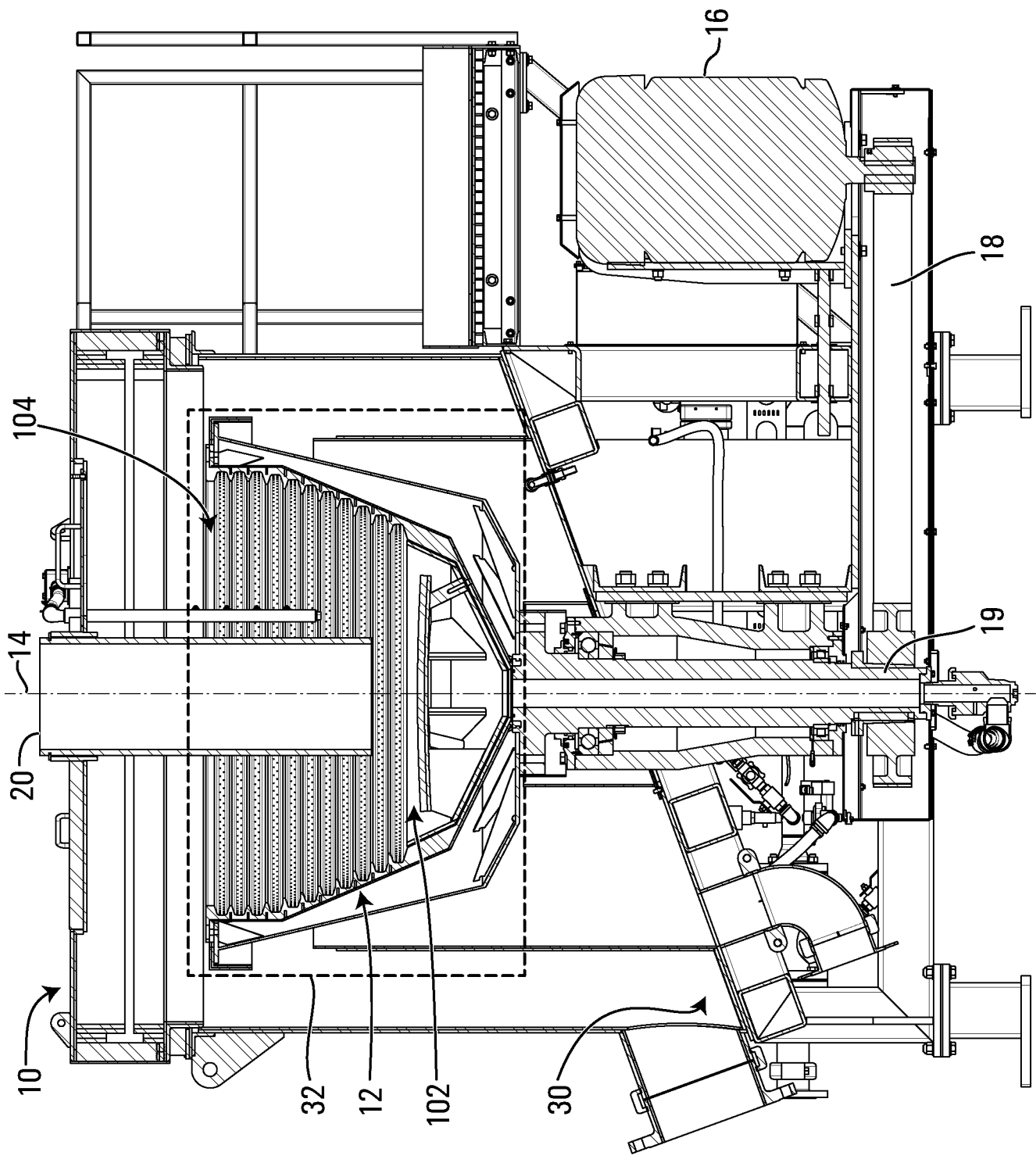
the apparatus of any one of claims **1** to **20**;

a rotation driver coupled to the apparatus for causing the separator of the apparatus to rotate about the rotation axis; and

10 a particle source in particle communication with the input end of the separator and configured to provide particles to the input end of the separator while the separator rotates about the rotation axis.

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FIG. 1



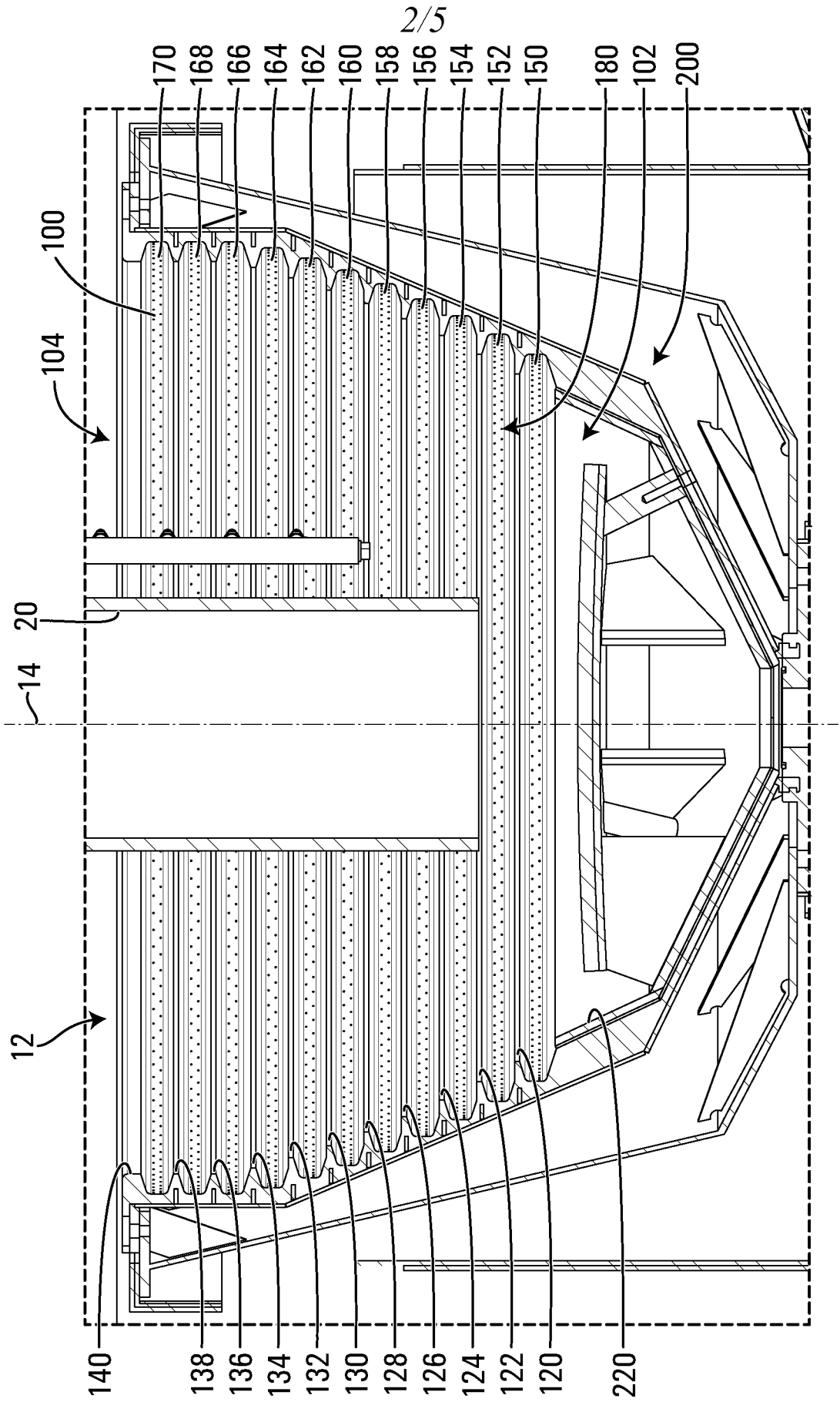


FIG. 2

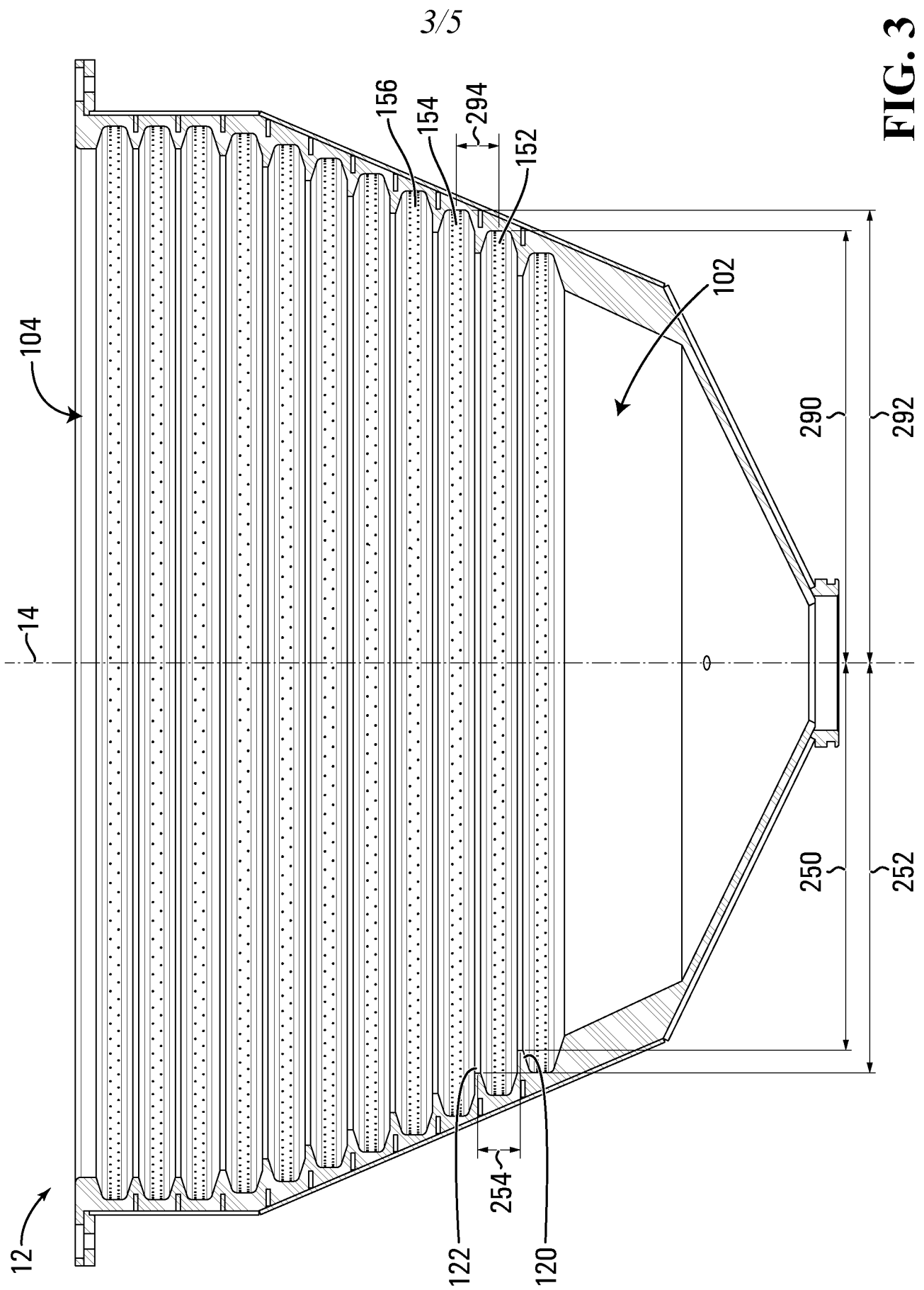


FIG. 3

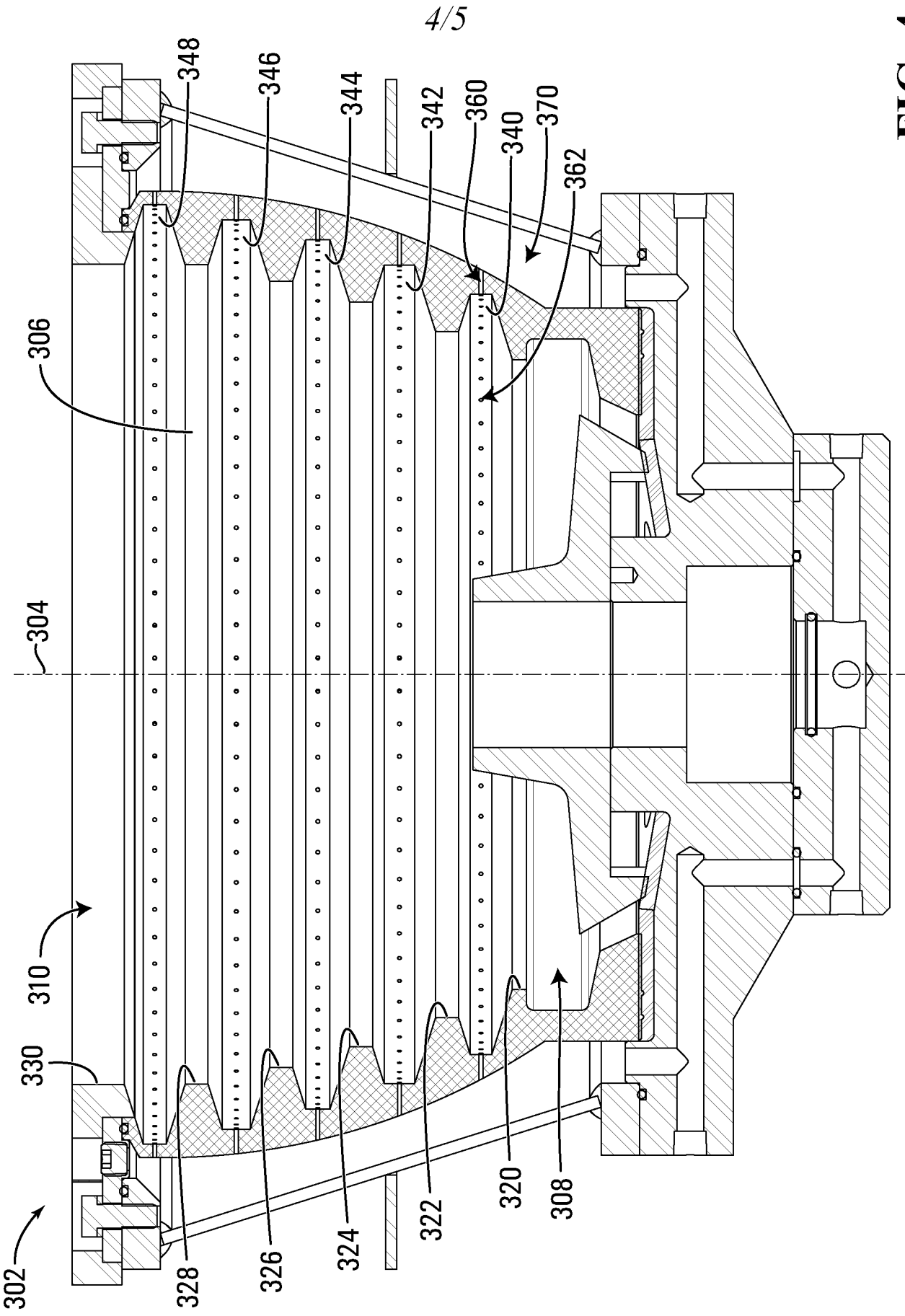


FIG. 4

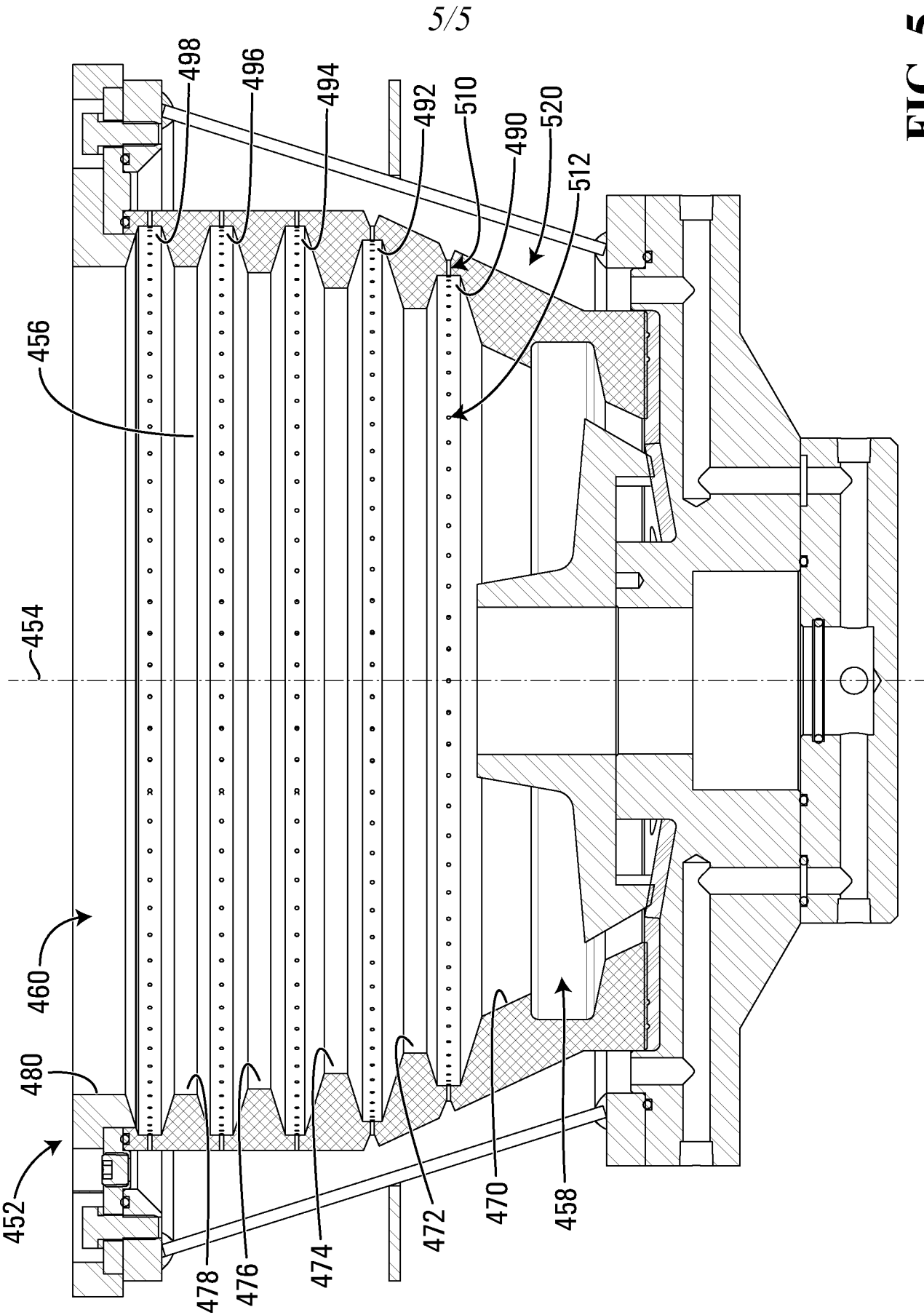


FIG. 5

INTERNATIONAL SEARCH REPORT

International application No.

PCT/CA2021/050528A. CLASSIFICATION OF SUBJECT MATTER
IPC: **B01D 21/26** (2006.01)

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: B01D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database(s) consulted during the international search (name of database(s) and, where practicable, search terms used)

Canadian patent database, Questel Orbit, Scopus, Google
KW- separation, density, particle, rotation, slope, bowl

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	CA 2140551 (Knelson) 17 February 1994 (17-02-1994)	1-21
A	CA 1301725 (Knelson) 26 May 1992 (26-05-1992)	1-21
A	CA 2271958 (Knelson) 18 June 1998 (18-06-1998)	1-21

☐ Further documents are listed in the continuation of Box C.☒ See patent family annex.

* "A" "D" "E" "L" "O" "P"	Special categories of cited documents: document defining the general state of the art which is not considered to be of particular relevance document cited by the applicant in the international application earlier application or patent but published on or after the international filing date document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) document referring to an oral disclosure, use, exhibition or other means document published prior to the international filing date but later than the priority date claimed	"T" "X" "Y" "&"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art document member of the same patent family
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Date of the actual completion of the international search
10 June 2021 (10-06-2021)Date of mailing of the international search report
15 July 2021 (15-07-2021)Name and mailing address of the ISA/CA
Canadian Intellectual Property Office
Place du Portage I, C114 - 1st Floor, Box PCT
50 Victoria Street
Gatineau, Quebec K1A 0C9
Facsimile No.: 819-953-2476

Authorized officer

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INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.
PCT/CA2021/050528

Patent Document Cited in Search Report	Publication Date	Patent Family Member(s)	Publication Date
CA2140551A1	17 February 1994 (17-02-1994)	CA2140551A1 CA2140551C AT178813T AU4692993A AU677217B2 BR9306822A DE69324491D1 DE69324491T2 EP0651676A1 EP0651676B1 ES2133406T3 RU95110760A RU2116841C1 US5338284A WO9403277A1	17 February 1994 (17-02-1994) 22 September 1998 (22-09-1998) 15 April 1999 (15-04-1999) 03 March 1994 (03-03-1994) 17 April 1997 (17-04-1997) 08 December 1998 (08-12-1998) 20 May 1999 (20-05-1999) 18 November 1999 (18-11-1999) 10 May 1995 (10-05-1995) 14 April 1999 (14-04-1999) 16 September 1999 (16-09-1999) 10 June 1997 (10-06-1997) 10 August 1998 (10-08-1998) 16 August 1994 (16-08-1994) 17 February 1994 (17-02-1994)
CA1301725C	26 May 1992 (26-05-1992)	CA1301725C AU3615389A AU616529B2	26 May 1992 (26-05-1992) 14 December 1989 (14-12-1989) 31 October 1991 (31-10-1991)
CA2271958C	08 February 2000 (08-02-2000)	CA2271958C AR010687A1 AU5185798A AU719402B2 BR9713687A ID18583A PE3899A1 US5795014A US5895345A WO9825705A1 ZA9710929B	08 February 2000 (08-02-2000) 28 June 2000 (28-06-2000) 03 July 1998 (03-07-1998) 11 May 2000 (11-05-2000) 28 March 2000 (28-03-2000) 23 April 1998 (23-04-1998) 22 February 1999 (22-02-1999) 18 August 1998 (18-08-1998) 20 April 1999 (20-04-1999) 18 June 1998 (18-06-1998) 06 September 1999 (06-09-1999)